# Lutheran Church of The Good Shepherd Request for Solar Quote (RFQ)



# Issued by Olympia Community Solar

Mason Rolph Olympia Community Solar 112 4th Ave E, STE 208 Olympia WA, 98501 (360) 481-4020 mason@olysol.org

Keith Folkerts Solar Project Lead olyoak@gmail.com (360) 731-8644



# REQUEST FOR QUOTE FOR INSTALLATION OF A SOLAR PROJECT

# **Summary**

Good Shepherd, with the support of Olympia Community Solar, is seeking a quote from a qualified firm to install a commercial solar energy installation in late 2023. Olympia Community Solar is supporting the Church to develop the solar project on the non-profit owned and occupied property.

# SITE VISIT

Project partners will host a site visit on November 18th at 9:00 AM PST.

# SITE ADDRESS

1601 North St SE, Olympia, WA 98501

# PROPOSAL SUBMITTAL

Please submit a proposal in PDF form to the points of contact by 5:00pm on December 16th.

# BASIC REQUIREMENTS FOR PROPOSING FIRMS

- Must be registered, or indicate that they will register, with the appropriate Business License divisions in Thurston County and in good standing to be considered for this project.
- Must be a general contractor and must hold an active Contractor Registration with Washington State Department of Labor and Industries.
- Must prove and maintain Workers' Compensation and Employer's Liability insurance.

Site Visits	November 18th at 9:00 AM
Proposals Due	December 16th by 5:00 PM
Firm Selected	December 23rd
Installation Work Start	Q4 2023

# PROPOSAL FORMAT AND EVALUATION CRITERIA

Please create project proposals in 8½" x 11" document size using a minimum 12-point font size. Proposals shall not exceed 15 pages, including cover page, cover letter and any appendices and/ or attachments.

# I. Cover letter

**A.** The cover letter shall discuss the highlights, key features and distinguishing points of the Proposal. The cover letter must be prepared and signed by a manager having the authority to make offers and enter into financial agreements on behalf of the firm.

# II. Proposing firm profile

**A.** Detail the proposing firm's size and local organizational structure. Describe the demonstrated experience of the firm in designing and installing commercial solar electric systems. Please note any significant installations by the firm in Thurston County.

# III. Qualifications of the project team

- **A.** Identify key personnel for this project including roles, experience, licenses, and certificates (e.g., NABCEP), with corresponding numbers as appropriate. Key personnel should include at a minimum: Owners/Principals; Project Managers; Designers; Installers.
- **B.** Identify any subcontractors the firm plans to use.

# IV. Business practices

- A. **Work practices**: Address the firm's health and safety record and practices. Identify any communications with the Washington State Department of Labor and Industries and state or federal human rights agencies regarding workplace issues in the last 3 years.
- B. **Liability**: Provide information on the level of insurance the firm has and provide copies of certificates.
- C. **Workmanship Warranties:** Describe your workmanship warranties.
- D. **Wages and Labor Practices:** Provide information about labor practices, including your commitment to providing family wages, benefits, apprenticeships, or mentoring programs.

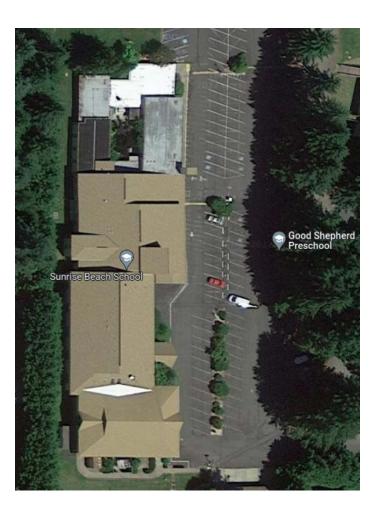
# V. Work quality

**A.** Explain why the products included in the proposal are appropriate for this project.

- **B.** Provide descriptions of warranties and support that ensure the long-term durability, operation, and maintenance of PV installations. Please describe any system monitoring capabilities or production gauges included. **Please attach the manufacturer's specification sheets and warranty information for each major piece of equipment.** Please indicate the equipment's location of origin.
- **C.** Include a solar production estimate. If the proposal includes modules on multiple different roof orientations, please factor each orientation into your production estimate.

# VI. <u>Customer service</u>

- **A.** Describe how the firm plans to handle incident reports (trouble, warranty, service calls, and inquiries). Discuss the firm's typical response time on calls, hours of coverage for customer service calls, and process for providing status reports after an incident is logged.
- **B.** List any complaints received by the Better Business Bureau or the Washington Attorney General's office over the last 3 years.
- **C.** Describe the training the firm provides the host including materials or manuals, customer care books, and/or support for later questions and system performance.



# EXHIBIT A Good Shepherd Lutheran Church

Founded in 1957, the church on the corner of North and Henderson streets has grown and changed over the years. As the building has expanded, so has its outreach, most recently with outdoor Sunday morning worship under the cathedral of evergreens on the church's six acres. Under the current leadership of Pastor Carol Tomer and Pastor Melissa Anderson Trust and a growing staff and newly forming ministry teams, the congregation is moving into its next chapter of ministry, called The Good Courage Journey.

The congregation is an open-hearted, open-minded ELCA congregation. Of particular note is that it has been a Reconciling in Christ congregation since 2009, meaning that it is publicly welcoming of LGBTQ people, as well as being deeply involved in an expansive ministry of justice-making and mercy. This wide-reaching commitment is proclaimed in these words:

"The Lutheran Church of The Good Shepherd welcomes all people: the poor and the rich, the young and the old; people who are single, married, blessed, divorced, separated, partnered or widowed; people of all abilities; people of all sexual orientations and gender identities; people of all nations and ethnic backgrounds. No matter who you are or where you are on life's journey, you are welcome here."

The current ministries of the congregation include a newly debuting contemplative evening service at dusk under the trees on each Thursday in August. This is made possible because Good Shepherd has just been named a Calvin Vital Worship Grant recipient, one of 13 congregations in North America this year. Fridays with Friends will offer intergenerational activities for children, youth, and all ages through the summer. A quilting group (called the Piece Corp) makes and sends around the world (through Lutheran World Relief) over 400 quilts each year. The congregation has a community garden that is used by members and the local community, and its harvests are contributed to the local food banks. The church has been a hub of the community, hosting in its building several other organizations: CIELO (Olympia Latino Comprehensive Educational Center), Scouts, Sunrise Beach School, basketball, soccer, and pickleball groups, theater groups, local music recitals, support groups, the Olympia School District's Transition Academy, as well as the CIELO Food and Hygiene Supply Bank.

# **Electricity Consumption**

Good Shepherd is serviced through a single PSE meter (Rate Schedule Commercial 24).

In 2021 the church consumed about 145 MWhs.

In 2022 the church consumed about 112.2 MWhs. Electric bill attached.

# **Load Capacity**

In preparation for this solicitation, th church commissioned a load capacity assessment of their roofs, which confirmed that they are adequate for a solar installation. Load Assessment attached.



Important Information

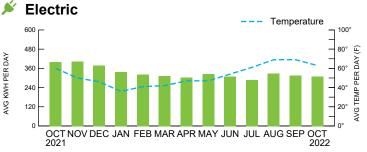
pse.com



# **LUTHERAN CHURCH**

Serving: 1601 NORTH ST SE, Olympia

# Your Usage Information



	Last Year	This Year
Average daily kilowatt hours	397.50	307.50
Average daily cost	\$47.06	\$36.60
Days in billing cycle	32	32
Average temperature	60°F	63°F

# **Your Account Summary**

**Previous Charges:** 

Amount of Your Last Bill (dated 9/6/2022) 1,110.09 Payment received 9/26/2022 - Thank you! -1,110.09\$ **Total Previous Charges** 0.00 **Current Charges:** Electric Charges 1,171.26 \$ 1,171.26 **Total Current Charges** Total \$ Total includes current and past due charges 1.171.26

A bank withdrawal is scheduled for 10/26/2022 for charges due.

Late Payments | A late payment fee of 1% per month will apply to past due charges, if any, and amounts unpaid more than 10 business days after the statement due date. Amounts will be considered delinquent if payment is not received on or before the due date.

## Customer service, guaranteed

We stand behind our service, from keeping scheduled appointments to restoring power outages as soon as we can. We'll credit your bill if we fail to meet our service guarantees. pse.com/guarantees.

### How to reach us

For self-service options visit our website at pse.com.

🔀 Email: customercare@pse.com

Customer Service: 1-888-225-5773 TTY: 1-800-962-9498 Hours: 7:30 a.m. - 6:30 p.m. M - F TRS: 1-866-831-5161 Puget Sound Energy: P.O. Box 91269, Bellevue, WA 98009

24 Hour Emergency and Outage line: 1-888-225-5773



## Your Ways to Pay

TUMWATER WA 98501-3666

pse.com to pay online or to find pay station locations

Mail this coupon and make check payable to Puget Sound Energy

26700 1 AV 0.452 010231 **LUTHERAN CHURCH** 1601 NORTH ST SE





\$1,171.26 will be withdrawn from your bank account on 10/26/2022

# Serving:

1601 NORTH ST SE, Olympia

# **Puget Sound Energy** P.O. BOX 91269

Bellevue, WA 98009-9269

પ્લાન માં ત્યાર કર્યા કર્ય Your bill includes charges for electricity and/or natural gas, delivery services, general administration and overhead, metering, taxes, conservation expenses and other items.

# **№** Electric Detail Information: 1601 NORTH ST SE, Olympia, CHURCH

Rate Schedule	Meter#	Start Date	End Date	Multiplier	Kilowatt	Electric	Reactive	Meter
Nate Scriedule	ivietei #	Read	Read	iviuitipilei	Hours (kWh)	Demand (kW)	Power (kVAR)	Read Type
Commercial 24	D166220602	9/2	10/4	120	0.940			Actual Bood
Commercial 24	P166329693	661	743	120	9,840	540 —	_	Actual Read

Your Electric Charge Details (32 days)	Rate	x Unit	=	Charge	Definitions
9,840 kWh used for service 9/3/2022 - 10/4/2022					Basic Charge — Covers the costs for meters, meter
Basic Charge	\$25.95	per month	\$	25.95	reading, billing and other costs that do not vary with energy use or the number of days covered by the bill.
Electric Energy Charge (9/3/2022 - 9/30/2022)	0.096940	8,610 kWh		834.65	<b>Multiplier</b> — Converts the amount of electricity used as
Electric Energy Charge (10/1/2022 - 10/1/2022)	0.100209	307.44 kWh		30.81	measured by your meter into kWh.
Electric Energy Charge (10/2/2022 - 10/4/2022)	0.101514	922.56 kWh		93.65	<b>kWh</b> — Your use of electricity is billed in units called
Other Electric Charges & Credits					kilowatt hours. It is a unit of energy that equals 1,000 watts of electricity consumed in one hour.
Electric Cons. Program Charge	0.004827	9,840 kWh		47.50	Energy Exchange Credit — Federal Columbia River
Power Cost Adjustment	0.005604	9,840 kWh		55.14	Benefits supplied by Bonneville Power Administration
Merger Credit	0.000000	9,840 kWh		0.00	from low-cost power generated by federal hydroelectric dams.
Federal Wind Power Credit	-0.001423	9,840 kWh		-14.00	Other Electric Charges and Credits — Includes the
Renewable Energy Credit	-0.000021	9,840 kWh		-0.21	Conservation Program and Power Cost Adjustment (if
Subtotal				1,073.49	any) charges, and the Merger, Federal Wind Power, and Renewable Energy credits.
Taxes					
State Utility Tax (\$41.58 included in above charges)	3.873%				
Effect of Olympia City Tax	9.108%	\$1,073.49		97.77	
Current Electric Charges			\$	1,171.26	

A rate change became effective during this billing period. The listed rate item(s) that changed shows the dates, prices and charges for each portion of the bill period when they were in effect. Copies of the rate schedules are available upon request.

Your electric bill reflects changes in rates that went into effect on October 2, 2022.

# Emergency or Power Outage Dial 1-888-225-5773

To report a natural gas or electric emergency or a power outage, 24 hours a day, call **1-888-225-5773** 

Para informar sobre emergencias eléctricas, de gas o apagones 24 horas al día, llame al **1-888-225-5773** 

若欲報告天然氣或電氣突發事件,或停電事故,每天 24 小時均可致電 1-888-225-5773

Чтобы сообщить об аварии, связанной с природным газом или электроэнергией, или о перерыве в подаче электроэнергии, звоните в любое время суток по номеру **1-888-225-5773** 

We can translate for other languages. Call 1-888-225-5773.

### Keeping our word.

You will receive a \$50 credit on your PSE bill if we do not keep a set appointment to install new or reconnect existing service or inspect natural gas equipment. Exceptions apply during major storms or significant events beyond our control.

### You deserve excellent service.

Every day we aim to give you clear, understandable answers to your questions about bills, credits, deposits and your energy service. If you have a complaint or dispute with your bill or service, please call us at 1-888-225-5773. If you are not satisfied with the response, ask to speak with a supervisor. If you are still not satisfied, you may contact the Consumer Affairs section of the Utilities and Transportation Commission at 1-888-333-WUTC (9882) or complete an online complaint form at www.utc.wa.gov.

# STRUCTURAL CALCULATIONS

**FOR** 

SOLAR PANEL INSTALLATION 1601 NORTH ST. SE OLYMPIA WA. 98501

SITE SPECIFIC
VERTICAL
ANALYSIS AND DESIGN
(DO NOT REUSE)

FOR GOOD SHEPARD CHURCH

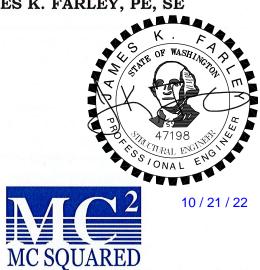
PROJECT #2022-0507

BY MC SQUARED, INC.

WILLIAM A. WITKOP, EIT

REVIEWED BY JAMES K. FARLEY, PE, SE

INCORPORATED



SCOPE: CLIENT REQUESTED STRUCTURAL ENGINEERING TO PROVIDE VERTICAL ENGINEERING FOR A SOLAR PANEL INSTALLATION THURSTON COUNTY, WA.

BASIS OF DESIGN IS DRAWINGS PROVIDED BY CLIENT. NO ANALYSIS AND DESIGN OF BRACING, TEMPORARY OR PERMANENT, REQUESTED OR CONDUCTED. ALL BRACING, TEMPORARY AND PERMANENT, SHALL BE RESPONSIBILITY OF CONTRACTOR.

LOADS:

2018 IBC/ASCE 7-16

VERTICAL:

ROOF DL= 15 PSF

SL= Pg = 20 PSF, DESIGN = 25 PSF

SP= 3 PSF (SOLAR PANELS)

WIND:

2018 IBC, PER ASCE 7-16, SECTION 26.

RISK CATEGORY II, 103 MPH

EXPOSURE B. SEE ATTACHED WIND

CALCULATIONS.

APPROX. MEAN ROOF HT = 30'

# MC SQUARED, INC.

OLYMPIA, WASHINGTON 98506 (360) 754-9339 FAX (360) 352-2044

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Date: 10/19/2027 By: WAW

Sheet: RECOMMENDATIONS Page of

BASED ON THE ATTACHED CALCULATION PACKAGE, THE ROOF SUPPORTS OVER THE CLASSROOMS, SANCTUARY, AND GYMNASIUM HAVE SUFFICIENT CAPACITY TO ADD SOLAR PANELS IN THESE AREAS.

THE SOLAR PANELS MUST BE CONNECTED

TO THE ROOF WITH A MINIMUM

OF 30 PSF UPLIFT CAPACITY FROM WIND.

SOLAR PANEL SIZE AND LAY OUT PLAN.

REQUIRED TO PROVIDE UPLIFT CONNECTION

DESIGN.

⚠ This is a beta release of the new ATC Hazards by Location website. Please contact us with feedback.

The ATC Hazards by Location website will not be updated to support ASCE 7-22. Find out why.

# ATC Hazards by Location

# **Search Information**

Address:

1601 North Street SE, Olympia, WA 98501, USA

Coordinates:

47.0159813, -122.8798548

Elevation:

177 ft

Timestamp:

2022-10-04T16:04:59.743Z

Hazard Type:

Wind



ASCE 7-16		ASCE 7-10		ASCE 7-05	
MRI 10-Year	66 mph	MRI 10-Year 72	2 mph	ASCE 7-05 Wind Speed	85 mph
MRI 25-Year	72 mph	MRI 25-Year 79	mph mph		
MRI 50-Year	77 mph	MRI 50-Year 85	5 mph		
MRI 100-Year	82 mph	MRI 100-Year 91	mph		
Risk Category I	91 mph	Risk Category I 100	) mph		
Risk Category II	97 mph	Risk Category II 110	) mph		
Risk Category III	103 mph	Risk Category III-IV 115	mph		
Risk Category IV	107 mph				

The results indicated here DO NOT reflect any state or local amendments to the values or any delineation lines made during the building code adoption process. Users should confirm any output obtained from this tool with the local Authority Having Jurisdiction before proceeding with design.

Please note that the ATC Hazards by Location website will not be updated to support ASCE 7-22. Find out why.

# Disclaimer

Hazard loads are interpolated from data provided in ASCE 7 and rounded up to the nearest whole integer. Per ASCE 7, islands and coastal areas outside the last contour should use the last wind speed contour of the coastal area - in some cases, this website will extrapolate past the last wind speed contour and therefore, provide a wind speed that is slightly higher. NOTE: For queries near wind-borne debris region boundaries, the resulting determination is sensitive to rounding which may affect whether or not it is considered to be within a wind-borne debris region.

Mountainous terrain, gorges, ocean promontories, and special wind regions shall be examined for unusual wind conditions.

While the information presented on this website is believed to be correct, ATC and its sponsors and contributors assume no responsibility https://hazards.atcouncil.org/#/wind?lat=47.0159813&lng=-122.8798548&address=1601 North Street SE%2C Olympia%2C WA 98501%2C USA 1/2 or liability for its accuracy. The material presented in the report should not be used or relied upon for any specific application without competent examination and verification of its accuracy, suitability and applicability by engineers or other licensed professionals. ATC does not intend that the use of this information replace the sound judgment of such competent professionals, having experience and knowledge in the field of practice, nor to substitute for the standard of care required of such professionals in interpreting and applying the results of the report provided by this website. Users of the information from this website assume all liability arising from such use. Use of the output of this website does not imply approval by the governing building code bodies responsible for building code approval and interpretation for the building site described by latitude/longitude location in the report.

# MC SQUARED, INC.

OLYMPIA, WASHINGTON 98506 (360) 754-9339 FAX (360) 352-2044

7	177		17.
Job:	ULL	05	UP

Date: 10/4/2022 By: W. WITKOP

Sheet: WIND

RISK CATEGORY III - (ASCE 7-16 TABLE 1.5-1) WIND SPEED V = 103 MPY DESIGN 3-5 GUST (ASCE 7-16 TABLE 26.5-1C) EXPOSURE CATEGORY B- (ASCE 26.7.3) KZE = 1.0 - STRUCTURE NOT BUILT ON A HILL  $P_{s} = \lambda k_{zt} P_{s30}$  (ASCE 7 16 28 5-1) MEAN ROOF HEIGHT = 30'=h  $-6 = 23^{\circ}$   $\lambda = 1.0$  ASCE  $-P_{30} = -26.5$  PSF Ps=(1.0)(1.0)(-26-5: PSF7 = -26.5 PSF TRUSSES AT 9 FT O.C. >-26.5 PSFX9 FT=-238.5 PLF SOLAR PANEL CONNECTIONS TO ROOF MUST HAVE A MINIMUM CAPACITY OF 30 PSF UPLIFT STRENGTH

MC SQUARED, INC. OLYMPIA, WASHINGTON 98506 (360) 754-9339 FAX (360) 352-2044

Job:			
Date:	By:		
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TRUSSES OVER	CLASSROOM ARE 50	PACED AT
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	THE ADDITIONAL	
- PRESSURE ADDE	D BY THE SOLAR	PANELS
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# MC SQUARED, INC.

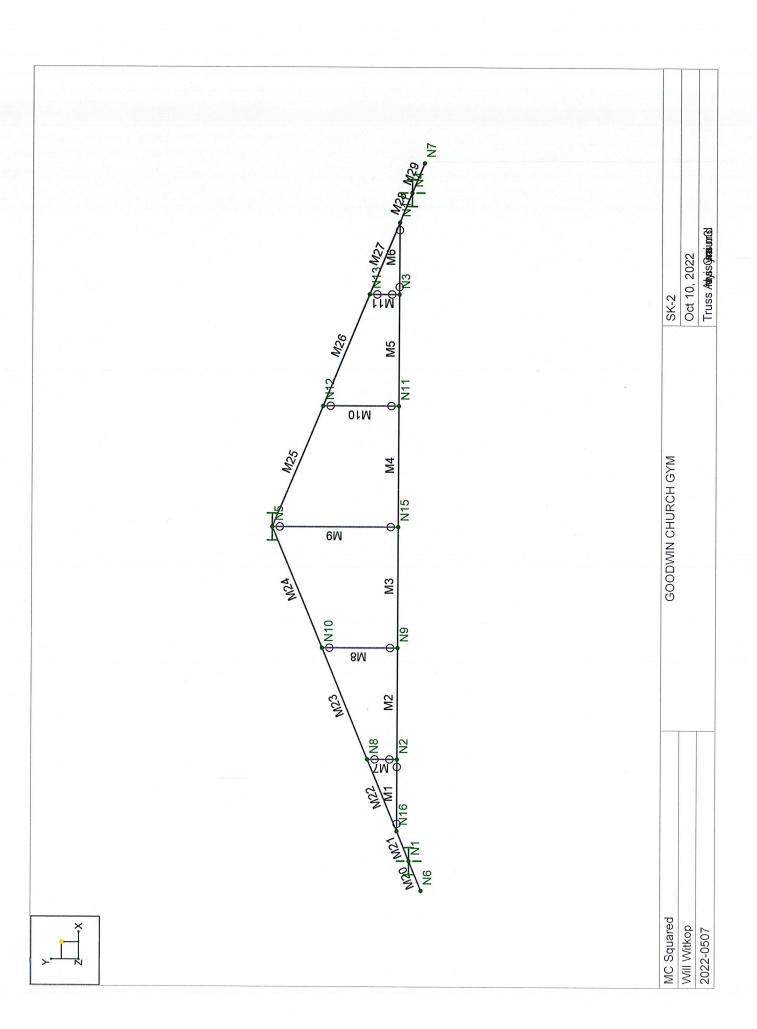
OLYMPIA, WASHINGTON 98506 (360) 754-9339 FAX (360) 352-2044

Job:_	2022	-050	クチ	

Date: 10/10/2027 By:

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FORCES AT GYM ROOF
DEAD LOAD = 135 PLF
- SNOW LOAD = ZZS PLF
WIND LOAD = -239 PLF (UPLIFT)
SOLAR PANELS = 27 PLF
_ DL + SL = 36 0 PLF
5P = Z7 PLF = 7.5% >5%
DL+SL 360 PLF
MORE CALCULATIONS NECESSARY





Company : MC Squared Designer : Will Witkop Job Number : 2022-0507

Model Name: GOODWIN CHURCH GYM

10/10/2022 4:30:37 PM

Checked By: JKF

# **Node Coordinates**

	Label	X [ft]	Y [ft]	Z [ft]	Detach From Diaphragm
1	N1	0	0	0	
2	N2	8.2	1	0	
3	N3	45.7	1	0	
4	N4	53.9	0	0	
5	N5	26.95	11.23	0	
6	N6	-2.4	-1	0	
7	N7	56.3	-1	0	
8	N8	8.2	3.416968	0	
9	N9	17.2	1	0	
10	N10	17.2	7.167223	0	
11	N11	36.7	1	0	
12	N12	36.7	7.167223	0	
13	N13	45.7	3.416968	0	
14	N15	26.95	1	0	
15	N16	2.399673	1	0	
16	N17	51.500327	1	0	

Node Boundary Conditions

	Node Label	X [k/in]	Y [k/in]	Z [k/in]	X Rot [k-ft/rad]
1	N11			Reaction	
2	N9			Reaction	
3	N1	Reaction	Reaction	Reaction	Reaction
4	N5			Reaction	Reaction
5	N4		Reaction	Reaction	Reaction

Wood Properties

	Label	Туре	Database	Species	Grade C	n (	Ci	Emod	Nu -	Therm. Coeff. [15°F	Density [k/ft³]
1	DF	Solid Sawn	Visually Graded	Douglas Fir-Larch	No.1			1	0.3	0.3	0.035
2	SP	Solid Sawn	Visually Graded	Southern Pine	No.1			1	0.3	0.3	0.035
3	HF	Solid Sawn	Visually Graded	Hem-Fir	No.1			1	0.3	0.3	0.035
4	SPF	Solid Sawn	Visually Graded	Spruce-Pine-fir	No.1			1	0.3	0.3	0.035
5	24F-1.8E DF Balanced	Glulam	NDS Table 5A	24F-1.8E DF BAL	na			1	0.3	0.3	0.035
6	24F-1.8E DF Unbalanced	Glulam	NDS Table 5A	24F-1.8E DF UNBAL	na			1	0.3	0.3	0.035
7	24F-1.8E SP Balanced	Glulam	NDS Table 5A	24F-1.8E SP BAL	na			1	0.3	0.3	0.035
8	24F-1.8E SP Unbalanced	Glulam	NDS Table 5A	24F-1.8E SP UNBAL	na			1	0.3	0.3	0.035
9	1.3E-1600F_VERSALAM	SCL	Boise Cascade	1.3E-1600F VERSALAM	na			1	0.3	0.3	0.035
10	1.35E LSL SolidStart	SCL	Louisiana Pacific	1.35E LSL SolidStart	na			1	0.3	0.3	0.035
11	1.3E RIGIDLAM LVL	SCL	Roseburg Forest Products	1.3E RIGIDLAM LVL	na			1	0.3	0.3	0.035
12	2.0E DF Parallam PSL	SCL	TrusJoist	2.0E DF Parallam PSL	na			1	0.3	0.3	0.035
13	LVL PRL 1.5E 2250F	Custom	N/A	LVL PRL 1.5E 2250F	na			1	0.3	0.3	0.035
14	LVL_Microlam_1.9E_2600F	Custom	N/A	LVL_Microllam_1.9E_2600F	na			1	0.3	0.3	0.035
15	PSL_Parallam_2.0E_2900F	Custom	N/A	PSL_Parallam_2.0E_2900F	na			1	0.3	0.3	0.035
16	LSL_TimberStrand_1.55E_2325F	Custom	N/A	LSL_TimberStrand_1.55E_2325F	na			1	0.3	0.3	0.035

Hot Rolled Steel Properties

100	Label	E [ksi]	G [ksi]	Nu	Therm. Coeff. [18°F -1]	Density [k/ft³]	Yi el d	[ksi Ry	Fu [ksi]	Rt
1	A992	29000	11154	0.3	0.65	0.49	50	1.1	65	1.1
2	A36 Gr.36	29000	11154	0.3	0.65	0.49	36	1.5	58	1.2
3	A572 Gr.50	29000	11154	0.3	0.65	0.49	50	1.1	65	1.1
4	A500 Gr.B RND	29000	11154	0.3	0.65	0.527	42	1.4	58	1.3
5	A500 Gr.B RECT	29000	11154	0.3	0.65	0.527	46	1.4	58	1.3



Company : MC Squared Designer : Will Witkop Job Number : 2022-0507

Model Name: GOODWIN CHURCH GYM

10/10/2022 4:30:37 PM

Checked By: JKF

# Hot Rolled Steel Properties (Continued)

	Label	E [ksi]	G [ksi]	Nu	Therm. Coeff. [16°F -1]	Density [k/ft³]	Yi el d	[ksiRy	Fu [ksi]	Rt
6	A500 Gr.C RND	29000	11154	0.3	0.65	0.527	46	1.4	62	1.3
7	A500 Gr.C RECT	29000	11154	0.3	0.65	0.527	50	1.4	62	1.3
8	A53 Gr.B	29000	11154	0.3	0.65	0.49	35	1.6	60	1.2
9	A1085	29000	11154	0.3	0.65	0.49	50	1.4	65	1.3
10	A913 Gr.65	29000	11154	0.3	0.65	0.49	65	1.1	80	1.1

# Hot Rolled Steel Section Sets

Label	Shape	Туре	Design List	Material	Design Rule	Area [in²]	lyy [in⁴]	lzz [in⁴]	J [in⁴]
1 HR1	GYMNASIUMBARS	HBrace	BAR	A36 Gr.36	Typical	0.785	0.049	0.049	0.098
2 HR2	HR2	HBrace	BAR	A36 Gr.36	Typical	2.461	0.482	0.482	0.964

# **Wood Section Sets**

	Label	Shape	Туре	Design List	Material	Design Rule	Area [in²]	lyy [in⁴]	lzz [in⁴]	J [in⁴]
1	W1	6.75X9FS	Beam	Glulam Western	24F-1.8E SP Balanced	Typical	60.75	230.66	410.062	498.188
2	W2	6.75X18FS	Beam	Glulam Western	24F-1.8E SP Balanced	Typical	121.5	461.32	3280.5	1410.052

Wood Design Parameters

	Label	Shape	Length [ft]	le-bend top [ft]	Cr	y sway	z sway
1	M2	W1	9	Lbyy			
2	M20	W2	2.6	Lbyy			
3	M21	W2	2.6	Lbyy			
4	M22	W2	6.284	Lbyy			
5	M23	W2	9.75	Lbyy			
6	M24	W2	10.563	Lbyy			
7	M25	W2	10.563	Lbyy			
8	M26	W2	9.75	Lbyy			
9	M27	W2	6.284	Lbyy			
10	M28	W2	2.6	Lbyy			
11	M29	W2	2.6	Lbyy			
12	M3	W1	9.75	Lbyy			
13	M4	W1	9.75	Lbyy			
14	M5	W1	9	Lbyy			

Hot Rolled Steel Design Parameters

	Label	Shape	Length [ft]	Lcomp top [ft]	Channel Conn.	a [ft]	Function
1	M1	HR2	5.8	Lbyy	N/A	N/A	Lateral
2	M6	HR2	5.8	Lbyy	N/A	N/A	Lateral
3	M7	HR1	2.417	Lbyy	N/A	N/A	Lateral
4	M8	HR1	6.167	Lbyy	N/A	N/A	Lateral
5	M10	HR1	6.167	Lbyy	N/A	N/A	Lateral
6	M11	HR1	2.417	Lbyy	N/A	N/A	Lateral
7	M9	HR1	10.23	Lbvv	N/A	N/A	Lateral

# Member Distributed Loads (BLC 1 : DL)

	Member Label	Direction	Start Magnitude [k/ft, F, ksf,-ft/ft]	End Magnitude [k/ft, F, ksf,-ft/ft]	Start Location [(ft, %)]	End Location [(ft, %)]
1	M20	Y	-0.135	-0.135	0	%100
2	M21	Υ	-0.135	-0.135	0	%100
3	M22	Υ	-0.135	-0.135	0	%100
4	M23	Υ	-0.135	-0.135	0	%100



Company : MC Squared Designer : Will Witkop Job Number : 2022-0507

Model Name: GOODWIN CHURCH GYM

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# Member Distributed Loads (BLC 1 : DL) (Continued)

	Member Labe	<b>Direction</b>	Start Magnitude [k/ft, F, ksf,-fk/ft]	End Magnitude [k/ft, F, ksf,-ft/ft]	Start Location [(ft, %)]	End Location [(ft, %)]
5	M24	Υ	-0.135	-0.135	0	%100
6	M25	Υ	-0.135	-0.135	0	%100
7	M26	Υ	-0.135	-0.135	0	%100
8	M27	Υ	-0.135	-0.135	0	%100
9	M28	Υ	-0.135	-0.135	0	%100
10	M29	Υ	-0.135	-0.135	0	%100

# Member Distributed Loads (BLC 2 : SL)

	Member Labe	el Direction	Start Magnitude [k/ft, F, ksf,-fk/ft]	End Magnitude [k/ft, F, ksf,-ft/ft]	Start Location [(ft, %)]	End Location [(ft, %)]
1	M20	Υ	-0.225	-0.225	0	%100
2	M21	Υ	-0.225	-0.225	0	%100
3	M22	Y	-0.225	-0.225	0	%100
4	M23	Y	-0.225	-0.225	0	%100
5	M24	Y	-0.225	-0.225	0	%100
6	M25	Υ	-0.225	-0.225	0	%100
7	M26	Y	-0.225	-0.225	0	%100
8	M27	Υ	-0.225	-0.225	0	%100
9	M28	Υ	-0.225	-0.225	0	%100
10	M29	Υ	-0.225	-0.225	0	%100

# Member Distributed Loads (BLC 3 : SP)

	Member Labe	el Direction	Start Magnitude [k/ft, F, ksf,-fk/ft]	End Magnitude [k/ft, F, ksf,-fl/ft]	Start Location [(ft, %)]	End Location [(ft, %)]
1	M20	Υ	-0.027	-0.027	0	%100
2	M21	Υ	-0.027	-0.027	0	%100
3	M22	Υ	-0.027	-0.027	0	%100
4	M23	Υ	-0.027	-0.027	0	%100
5	M24	Y	-0.027	-0.027	0	%100
6	M25	Υ	-0.027	-0.027	0	%100
7	M26	Υ	-0.027	-0.027	0	%100
8	M27	Υ	-0.027	-0.027	0	%100
9	M28	Y	-0.027	-0.027	0	%100
10	M29	Y	-0.027	-0.027	0	%100

# Member Distributed Loads (BLC 4: WL)

	Member Labe	el Direction	Start Magnitude [k/ft, F, ksf,-fk/ft]	End Magnitude [k/ft, F, ksf,-fl/ft]	Start Location [(ft, %)]	End Location [(ft, %)]
1	M20	Y	0.238	0.238	0	%100
2	M21	Y	0.238	0.238	0	%100
3	M22	Y	0.238	0.238	0	%100
4	M23	Y	0.238	0.238	0	%100
5	M24	Y	0.238	0.238	0	%100
6	M25	Y	0.238	0.238	0	%100
7	M26	Y	0.238	0.238	0	%100
8	M27	Y	0.238	0.238	0	%100
9	M28	Y	0.238	0.238	0	%100
10	M29	Υ	0.238	0.238	0	%100

# **Basic Load Cases**

	BLC Description	Category	Point	Distributed
1	DL	None		10
2	SL	None		10



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# Basic Load Cases (Continued)

	BLC Description	Category	Point	Distributed
3	SP	None		10
4	WL	None		10
9		None	1	

# **Load Combinations**

	Description	Solve	P-Delta	BLC	Factor	BLC	Factor	BLC	Factor
1	DL	Yes	Y	1	1				
2	DL+SL	Yes	Y	1	1	2	1		
3	DL+.6WL	Yes	Y	1	1	4	0.6		
4	DL+.75(.6)WL+.75SL	Yes	Y	1	1	4	0.45	2	1
5	SP	Yes	Y	3	1				
6	.6DL+.6WL	Yes	Y	1	0.6	4	0.6		
7	DL+SL+SP	Yes	Y	1	1	2	1	3	1

# Load Combination Design

	Description	CD	Service	Hot Rolled	Cold Formed	Wo o d	Concrete	Masonry	Aluminum	Stainless	Connection
1	DL			Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
2	DL+SL	1.15		Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
3	DL+.6WL	1.6		Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
4	DL+.75(.6)WL+.75SL	1.6		Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
5	SP			Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
6	.6DL+.6WL	1.6		Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
7	DL+SL+SP	1.15		Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes

# **Node Reactions**

	LC	Node Label	X [k]	Y [k]	Z [k]	MX [k-ft]	MY [-lft]	MZ [k-ft]
1	1	N11	0	0	0	0	0	0
2	1	N9	0	0	0	0	0	0
3	1	N1	0	4.292	0	0	0	0
4	1	N5	0	0	0	0	0	0
5	1	N4	0	4.292	0	0	0	0
6	1	Totals:	0	8.585	0			
7	1	COG (ft):	X: 26.95	Y: 5.115	Z: 0			
8	2	N11	0	0	0	0	0	0
9	2	N9	0	0	0	0	0	0
10	2	N1	0	11.447	0	0	0	0
11	2	N5	0	0	0	0	0	0
12	2	N4	0	11.447	0	0	0	0
13	2	Totals:	0	22.893	0			
14	2	COG (ft):	X: 26.95	Y: 5.115	Z: 0			
15	3	N11	0	0	0	0	0	0
16	3	N9	0	0	0	0	0	0
17	3	N1	0	-0.258	0	0	0	0
18	3	N5	0	0	0	0	0	0
19	3	N4	-0	-0.258	0	0	0	0
20	3	Totals:	0	-0.515	0			
21	3	COG (ft):	X: 26.95	Y: 5.115	Z: 0			
	4	N11	0	0	0	0	0	0
23	4	N9	0	0	0	0	0	0
24	4	N1	0	8.034	0	0	0	0
22 23 24 25 26	4	N5	0	0	0	0	0	0
26	4	N4	0	8.034	0	0	0	0



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# Node Reactions (Continued)

	LC	Node Label	X [k]	Y [k]	Z [k]	MX [k-ft]	MY [-lft]	MZ [k-ft]
27	4	Totals:	0	16.068	0	Control State Care		
28 <b>29</b>	4	COG (ft):	X: 26.95	Y: 5.115	Z: 0			
29	5	N11	0	0	0	0	0	0
30	5	N9	0	0	0	0	0	0
31	5	N1	0	0.858	0	0	0	0
32 33 34 35 36 37	5	N5	0	0	0	0	0	0
33	5	N4	0	0.858	0	0	0	0
34	5	Totals:	0	1.717	0			
35	5	COG (ft):	X: 26.95	Y: 5.115	Z: 0			
36	6	N11	0	0	0	0	0	0
37	6	N9	0	0	0	0	0	0
38 <b>39</b>	6	N1	0	-1.975	0	0	0	0
39	6	N5	0	0	0	0	0	0
40	6	N4	0	-1.975	0	0	0	0
41	6	Totals:	0	-3.949	0			
42	6	COG (ft):	X: 26.95	Y: 5.115	Z: 0			
43	7	N11	0	0	0	0	0	0
44	7	N9	0	0	0	0	0	0
45	7	N1	0	12.305	0	0	0	0
46	7	N5	0	0	0	0	0	0
47	7	N4	0	12.305	0	0	0	0
48	7	Totals:	0	24.61	0			
49	7	COG (ft):	X: 26.95	Y: 5.115	Z: 0			

Node Displacements

	LC	Node Label	X [in]	Y [in]	Z [in]	X Rotation [rad]	Y Rotation [	r ad]Z Rotation [rad]
1	1	N1	0	0	0	0	0	-3.182e-3
2	1	N2	0.046	-0.242	0	0	0	-4.616e-4
3	1	N3	0.074	-0.242	0	0	0	4.616e-4
4	1	N4	0.12	0	0	0	0	3.182e-3
5	1	N5	0.06	-0.172	0	0	0	0
6	1	N6	-0.038	0.091	0	0	0	-3.173e-3
7	1	N7	0.158	0.091	0	0	0	3.173e-3
8	1	N8	0.098	-0.242	0	0	0	-1.333e-3
9	1	N9	0.052	-0.258	0	0	0	5.114e-4
10	1	N10	0.101	-0.259	0	0	0	7.533e-4
11	1	N11	0.067	-0.258	0	0	0	-5.114e-4
12	1	N12	0.019	-0.259	0	0	0	-7.533e-4
13	1	N13	0.022	-0.242	0	0	0	1.333e-3
14	1	N15	0.06	-0.176	0	0	0	0
15	1	N16	0.038	-0.091	0	0	0	-2.917e-3
16	1	N17	0.082	-0.091	0	0	0	2.917e-3
17	2	N1	0	0	0	0	0	-8.515e-3
18	2	N2	0.122	-0.649	0	0	0	-1.23e-3
19	2	N3	0.199	-0.649	0	0	0	1.23e-3
20	2	N4	0.321	0	0	0	0	8.515e-3
21	2	N5	0.16	-0.459	0	0	0	0
22	2	N6	-0.102	0.245	0	0	0	-8.491e-3
23	2	N7	0.422	0.245	0	0	0	8.491e-3
24	2	N8	0.262	-0.648	0	0	0	-3.566e-3
25	2	N9	0.14	-0.689	0	0	0	1.367e-3
26	2	N10	0.269	-0.694	0	0	0	2.018e-3
27	2	N11	0.18	-0.689	0	0	0	-1.367e-3
28	2	N12	0.051	-0.694	0	0	0	-2.018e-3
29	2	N13	0.059	-0.648	0	0	0	3.566e-3



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# Node Displacements (Continued)

		Nada Labat		\/ r: 1	7	V D	\\ D	1375 4 4 5 13
	LC	Node Label	X [in]	Y [in]	Z [in]	X Rotation [rad]		r ad]Z Rotation [rad]
30	2	N15	0.16	-0.47	0	0	0	0
31	2	N16	0.1	-0.243	0	0	0	-7.806e-3
32	2	N17	0.22	-0.243	0	0	0	7.806e-3
33	3	N1	0	0	0	0	0	1.905e-4
34	3	N2	-0.003	0.015	0	0	0	2.77e-5
35	3	N3	-0.004	0.015	0	0	0	-2.77e-5
36	3	N4	-0.007	0	0	0	0	-1.905e-4
37	3	N5	-0.004	0.01	0	0	0	0
38	3	N6	0.002	-0.005	0	0	0	1.9e-4
39	3	N7	-0.009	-0.005	0	0	0	-1.9e-4
40	3	N8	-0.006	0.015	0	0	0	7.983e-5
41	3	N9	-0.003	0.015	0	0	0	-3.065e-5
42	3	N10	-0.006	0.016	0	0	0	-4.506e-5
43	3	N11	-0.004	0.015	0	0	0	3.065e-5
44	3	N12	-0.001	0.016	0	0	0	4.506e-5
45	3	N13	-0.001	0.015	0	0	0	-7.983e-5
46	3	N15	-0.004	0.011	0	0	0	0
47	3	N16	-0.002	0.005	0	0	0	1.746e-4
48	3	N17	-0.005	0.005	0	0	0	-1.746e-4
49	4	N1	0	0	0	0	0	-5.966e-3
50	4	N2	0.085	-0.455	0	0	0	-8.637e-4
51	4	N3	0.139	-0.455	0	0	0	8.637e-4
52	4	N4	0.225	0	0	0	0	5.966e-3
53	4	N5	0.112	-0.322	0	0	Ō	0
54	4	N6	-0.071	0.171	0	0	0	-5.949e-3
55	4	N7	0.296	0.171	Ō	0	0	5.949e-3
56	4	N8	0.183	-0.454	0	0	0	-2.499e-3
57	4	N9	0.098	-0.483	Ö	0	0	9.583e-4
58	4	N10	0.189	-0.486	0	0	0	1.413e-3
59	4	N11	0.126	-0.483	0	0	0	-9.583e-4
60	4	N12	0.036	-0.486	0	0	0	-1.413e-3
61	4	N13	0.041	-0.454	0	0	0	2.499e-3
62	4	N15	0.112	-0.33	0	0	0	0
63	4	N16	0.07	-0.17	0	0	0	-5.47e-3
64	4	N17	0.154	-0.17	0	0	0	5.47e-3
65	5	N1	0.104	0	0	0	0	-6.353e-4
66	5	N2	0.009	-0.048	0	0	0	-9.233e-5
67	5	N3	0.015	-0.048	0	0	0	9.233e-5
68	5	N4	0.013	0	0	0	0	6.353e-4
69	5	N5	0.012	-0.034	0	0	0	0.555e-4
70	5	N6	-0.008	0.018	0	0	0	-6.336e-4
71	5	N7	0.032	0.018	0	0	0	6.336e-4
72	5	N8	0.032	-0.048	0	0	0	-2.662e-4
73	5	N9	0.02	-0.048	0			
74		N10				0	0	1.022e-4
75	5		0.02 0.013	-0.052	0	0	0	1.503e-4
	5	N11		-0.051	0	0	0	-1.022e-4
76	5	N12	0.004	-0.052	0	0	0	-1.503e-4
77	5	N13	0.004	-0.048	0	0	0	2.662e-4
78	5	N15	0.012	-0.035	0	0	0	0
79	5	N16	0.007	-0.018	0	0	0	-5.825e-4
80	5	N17	0.016	-0.018	0	0	0	5.825e-4
81	6	N1	0	0	0	0	0	1.459e-3
82	6	N2	-0.021	0.111	0	0	0	2.124e-4
83	6	N3	-0.034	0.111	0	0	0	-2.124e-4
84	6	N4	-0.055	0	0	0	0	-1.459e-3



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# Node Displacements (Continued)

	LC	Node Label	X [in]	Y [in]	Z [in]	X Rotation [rad]	Y Rotation [r	ad]Z Rotation [rad]
85	6	N5	-0.028	0.079	0	0	0	0
86	6	N6	0.017	-0.042	0	0	0	1.455e-3
87	6	N7	-0.072	-0.042	0	0	0	-1.455e-3
88	6	N8	-0.045	0.111	0	0	0	6.116e-4
89	6	N9	-0.024	0.118	0	0	0	-2.348e-4
90	6	N10	-0.046	0.119	0	0	0	-3.451e-4
91	6	N11	-0.031	0.118	0	0	0 .	2.348e-4
92	6	N12	-0.009	0.119	0	0	0	3.451e-4
93	6	N13	-0.01	0.111	0	0	0	-6.116e-4
94	6	N15	-0.028	0.081	0	0	0	0
95	6	N16	-0.017	0.042	0	0	0	1.338e-3
96	6	N17	-0.038	0.042	0	0	0	-1.338e-3
97	7	N1	0	0	0	0	0	-9.157e-3
98	7	N2	0.131	-0.698	0	0	0	-1.323e-3
99	7	N3	0.214	-0.698	0	0	0	1.323e-3
100	7	N4	0.345	0	0	0	0	9.157e-3
101	7	N5	0.172	-0.494	0	0	0	0
102	7	N6	-0.11	0.263	0	0	0	-9.131e-3
103	7	N7	0.454	0.263	0	0	0	9.131e-3
104	7	N8	0.282	-0.697	0	0	0	-3.834e-3
105	7	N9	0.151	-0.741	0	0	0	1.47e-3
106	7	N10	0.29	-0.746	0	0	0	2.171e-3
107	7	N11	0.194	-0.741	0	0	0	-1.47e-3
108	7	N12	0.055	-0.746	0	0	0	-2.171e-3
109	7	N13	0.063	-0.697	0	0	0	3.834e-3
110	7	N15	0.172	-0.506	0	0	0	0
111	7	N16	0.108	-0.261	0	0	0	-8.395e-3
112	7	N17	0.237	-0.261	0	0	0	8.395e-3

# Member Section Forces

	LC	Member Label	Sec	Axial[k]	y Shear[k]	z Shear[k]	Tor que[k-ft]	y-y Moment[k-ft]	z-z Moment[k-ft]
1	1	M1	1	-6.539	0	0	0	0	0
2			2	-6.539	0	0	0	0	0
3			3	-6.539	0	0	0	0	0
4			4	-6.539	0	0	0	0	0
5			5	-6.539	0	0	0	0	0
6	1	M6	1	-6.539	0	0	0	0	0
7			2	-6.539	0	0	0	0	0
8			3	-6.539	0	0	0	0	0
9			4	-6.539	0	0	0	0	0
10			5	-6.539	0	0	0	0	0
11	1	M7	1	-0.102	0	0	0	0	0
12			2	-0.102	0	0	0	0	0
13			3	-0.102	0	0	0	0	0
14			4	-0.102	0	0	0	0	0
15			5	-0.102	0	0	0	0	0
16	1	M8	1	0.414	0	0	0	0	0
17			2	0.414	0	0	0	0	0
18			3	0.414	0	0	0	0	0
19			4	0.414	0	0	0	0	0
20			5	0.414	0	0	0	0	0
21	1	M10	1	0.414	0	0	0	0	0
22			2	0.414	0	0	0	0	0
23			3	0.414	0	0	0	0	0
24	ž :		4	0.414	0	0	0	0	0



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	LC	Member Label	Sec	Axial[k]	y Shear[k]	z Shear[k]	Tor que[k-ft]	y-y Moment[k-ft]	z-z Moment[k-ft]
25			5	0.414	0	0	0	0	0
26	1	M11	1	-0.102	0	0	0	0	0
27			2	-0.102	0	0	0	0	0
28			3	-0.102	0	0	0	0	0
29			4	-0.102	0	0	0	0	0
30			5	-0.102	0	0	0	0	0
31	1	M9	1	-0.58	0	0	0	0	0
32			2	-0.58	0	0	0	0	0
33			3	-0.58	0	0	0	0	0
34			4	-0.58	0	0	0	0	0
35			5	-0.58	0	0	0	0	0
36	1	M2	1	-6.538	0.123	0	0	0	0
37			2	-6.538	0.123	0	0	0	-0.277
38			3	-6.538	0.123	0	0	0	-0.554
39			4	-6.538	0.123	0	0	0	-0.831
40			5	-6.538	0.123	0	0	0	-1.108
41	_1_	M20	1	0	0	0	0	0	0
42		ESCHOLOGICAL CONTRACTOR	2	-0.034	-0.081	0	0	0	0.027
43			3	-0.067	-0.162	0	0	0	0.106
44			4	-0.101	-0.243	0	0	0	0.238
45			5	-0.135	-0.324	0	0	0	0.422
46	1	M21	1	1.516	3.645	0	0	0	0.422
47			2	1.482	3.565	0	0	0	-1.921
48			3	1.449	3.484	0	0	0	-4.211
49			4	1.415	3.403	0	0	0	-6.449
50		1400	5	1.381	3.322	0	0	0	-8.634
51	1	M22	1	7.408	0.803	0	0	0	-8.634
52			2	7.326	0.608	0	0	0	-9.742
53			3	7.245	0.412	0	0	0	-10.543
54			4	7.163	0.216	0	0	0	-11.036
55		1400	5	7.082	0.02	0	0	0	-11.222
56	1	M23	1	7.042	-0.097	0	0	0	-11.222
57			2	6.915	-0.401	0	0	0	-10.615
58			3	6.789	-0.705	0	0	0	-9.268
59			4	6.662	-1.008	0	0	0	-7.18
60	4	N40.4	5	6.536	-1.312	0	0	0	-4.352
61	1	M24	1	6.696	-0.939	0	0	0	-4.352
62 63			2	6.558	-1.268	0	0	0	-1.438
			3	6.421	-1.597	0	0	0	2.345
64 65			4	6.284	-1.926	0	0	0	6.997
66	1	MOE	5	6.147	-2.255	0	0	0	12.518
67	1	M25	2	6.147 6.284	2.255	0	0	0	12.518
68			3	6.421	1.926 1.597	0	0	0	6.997
69			4	6.421		0	0	0	2.345
70			5	6.696	1.268	0	0	0	-1.438
71	1	M26	1	6.536	0.939 1.312	0	0	0	-4.352
72		IVIZO	2	6.662	1.312			0	-4.352
73			3	6.789	0.705	0	0	0	-7.18
74			4	6.789	0.705			0	-9.268 10.615
75			5	7.042	0.401	0	0	0	-10.615
76	1	M27	1	7.042	-0.02			0	-11.222
77		IVIZ /	2	7.082	-0.02	0	0	0	-11.222
78			3	7.163	-0.412	0		0	-11.036
79	National State of the Control of the		4	7.245	-0.412	0	0	0	-10.543 -9.742



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	LC	Member Label	Sec	Axial[k]	y Shear[k]	z Shear[k]	Tor que[k-ft]	y-y Moment[k-ft]	z-z Moment[k-ft]
80			5	7.408	-0.803	0	0	0	-8.634
81	1	M28	1	1.381	-3.322	0	Ö	0	-8.634
82			2	1.415	-3.403	0	0	0	-6.449
83			3	1.449	-3.484	0	0	0	-4.211
84			4	1.482	-3.565	0	0	0	-1.921
85			5	1.516	-3.645	0	0	0	0.422
86	1	M29	1	-0.135	0.324	0	0	0	0.422
87			2	-0.101	0.243	0	0	0	0.238
88			3	-0.067	0.162	0	0	0	0.106
89			4	-0.034	0.081	0	0	0	0.027
90			5	0	0	0	0	0	0
91	1	M3	1	-6.539	-0.282	0	0	0	-1.108
92			2	-6.539	-0.282	0	0	0	-0.42
93			3	-6.539	-0.282	0	0	0	0.269
94			4	-6.539	-0.282	0	0	0	0.957
95			5	-6.539	-0.282	0	0	0	1.646
96	1	M4	1	-6.539	0.282	0	0	0	1.646
97			2	-6.539	0.282	0	0	0	0.957
98			3	-6.539	0.282	0	0	0	0.269
99			4	-6.539	0.282	0	0	0	-0.42
100			5	-6.539	0.282	0	0	0	-1.108
101	1	M5	1	-6.538	-0.123	0	0	0	-1.108
102			2	-6.538	-0.123	0	0	0	-0.831
103			3	-6.538	-0.123	0	0	0	-0.554
104			4	-6.538	-0.123	0	0	0	-0.277
105			5	-6.538	-0.123	0	0	0	0
106	2	M1	1	-17.462	0	0	0	0	0
107			2	-17.462	0	0	0	0	0
108			3	-17.462	0	0	0	0	0
109			4	-17.462	0	0	0	0	0
110			5	-17.462	0	0	0	0	0
111	2	M6	1	-17.462	0	0	0	0	0
112			2	-17.462	0	0	0	0	0
113			3	-17.462	0	0	0	0	0
114			4	-17.462	0	0	0	0	0
115			5	-17.462	0	0	0	0	0
116	2	M7	1	-0.176	0	0	0	0	0
117			2	-0.176	0	0	0	0	0
118			3	-0.176	0	0	0	0	0
119			4	-0.176	0	0	0	0	0
120			5	-0.176	0	0	0	0	0
121	2	M8	1	1.146	0	0	0	0	0
122			2	1.146	0	0	0	0	0
123			3	1.146	0	0	0	0	0
124			4	1.146	0	0	0	0	0
125			5	1.146	0	0	0	0	0
126	2	M10	1	1.146	0	0	0	0	0
127			2	1.146	0	0	0	0	0
128			3	1.146	0	0	0	0	0
129			4	1.146	0	0	0	0	0
130			5	1.146	0	0	0	0	0
131	2	M11	1	-0.176	0	0	0	0	0
132			2	-0.176	0	0	0	0	0
133			3	-0.176	0	0	0	0	0
134			4	-0.176	0	0	0	0	0



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	LC	Member Label	Sec	Axial[k]	y Shear[k]	z Shear[k]	Tor que[k-ft]	y-y Moment[k-ft]	z-z Moment[k-ft]
135			5	-0.176	0	0	0	0	0
136	2	M9	1	-1.613	0	0	0	0	0
137			2	-1.613	0	0	0	0	0
138			3	-1.613	0	0	0	0	0
139			4	-1.613	0	0	0	0	0
140			5	-1.613	0	0	0	0	0
141	2	M2	1	-17.461	0.329	0	0	0	0
142			2	-17.461	0.329	0	0	0	-0.74
143			3	-17.461	0.329	0	0	0	-1.479
144			4	-17.461	0.329	0	0	0	-2.219
145			5	-17.461	0.329	0	0	0	-2.958
146	2	M20	1	0	-0.002	0	0	0	0
147			2	-0.09	-0.218	0	0	0	0.072
148			3	-0.18	-0.434	0	0	0	0.284
149			4	-0.27	-0.65	0	Ö	0	0.637
150	A THE PARTY OF THE		5	-0.36	-0.866	0	0	0	1.13
151	2	M21	1	4.043	9.754	Ö	0	Ö	1.13
152			2	3.953	9.538	0	0	0	-5.14
153			3	3.863	9.322	0	0	0	-11.268
154			4	3.773	9.106	0	0	0	-17.257
155			5	3.683	8.89	o l	0	0	-23.105
156	2	M22	1	19.739	2.15	0	0	0	-23.105
157		IVIEE	2	19.521	1.628	0	0	0	-26.072
158			3	19.304	1.106	0	0	0	-28.22
159			4	19.086	0.584	0	0	0	-29.547
160			5	18.869	0.062	0	0	0	-30.054
161	2	M23	1	18.799	-0.268	0	0	0	-30.054
162	_	IVIZO	2	18.462	-1.078	0	0	0	-28.414
163			3	18.124	-1.888	0	0	0	-24.799
164			4	17.787	-2.698	0	0	0	-19.21
165			5	17.449	-3.508	0	0	0	-11.647
166	2	M24	1	17.893	-2.519	0	0	0	-11.647
167		IVIZ	2	17.527	-3.396	0	0	0	-3.837
168			3	17.162	-4.274	0	0	0	6.29
169			4	16.796	-5.151	0	0	0	18.734
170			5	16.43	-6.029	0	0	0	33.495
171	2	M25	1	16.43	6.029	0	0	0	33.495
172		IVIZU	2	16.796	5.151	0	0	0	18.734
173			3	17.162	4.274	0	0	0	6.29
174			4	17.102	3.396	0	0	0	-3.837
175			5	17.527	2.519	0	0	0	-11.647
176	2	M26	1	17.449	3.508				-11.647
177	2	IVIZU	2	17.787		0	0	0	-19.21
178			3	18.124	2.698 1.888	0	0	0	-24.799
179			4						
				18.462	1.078	0	0	0	<u>-28.414</u>
180 181	2	M27	5	18.799 18.869	0.268 -0.062	0	0	0	-30.054 -30.054
		IVIZ/							
182			2	19.086	-0.584	0	0	0	-29.547
183			3	19.304	-1.106	0	0	0	-28.22
184			4	19.521	-1.628	0	0	0	-26.072
185		MOO	5	19.739	-2.15	0	0	0	-23.105
186	2	M28	1	3.683	-8.89	0	0	0	-23.105
187			2	3.773	-9.106	0	0	0	-17.257
188	en e		3	3.863	-9.322	0	0	0	-11.268
189			4	3.953	-9.538	0	0	0	-5.14



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Checked By: JKF

	LC	Member Label	Sec	Axial[k]	y Shear[k]	z Shear[k]	Tor que[k-ft]	y-y Moment[k-ft]	z-z Moment[k-ft]
190	LO	Wichiber Laber	5	4.043	-9.754	0	0	0	1.13
191	2	M29	1	-0.36	0.866	Ö	0	0	1.13
192	_	WZO	2	-0.27	0.65	0	0	0	0.637
193			3	-0.18	0.434	0	0	0	0.284
194			4	-0.09	0.218	0	0	0	0.072
195			5	0	0.002	0	0	0	0.072
196	2	M3	1	-17.464	-0.754	0	0	0	-2.958
197		IVIO	2	-17.464	-0.754	0	0	0	-1.12
198			3	-17.464	-0.754	0	0	0	0.719
199			4	-17.464	-0.754	0	0	0	2.557
200			5	-17.464	-0.754	0	0		4.395
201	2	M4	1	-17.464	0.754	0	0	0	4.395
202		1014			0.754			The second secon	2.557
			2	-17.464		0	0	0	
203			3	-17.464	0.754	0	0	0	0.719
204			4	-17.464	0.754	0	0	0	-1.12
205	_	N 4 5	5	-17.464	0.754	0	0	0	-2.958
206	2	M5	1	-17.461	-0.329	0	0	0	-2.958
207			2	-17.461	-0.329	0	0	0	-2.219
208			3	-17.461	-0.329	0	0	0	-1.479
209			4	-17.461	-0.329	0	0	0	-0.74
210			5	-17.461	-0.329	0	0	0	0
211	3	M1	1	0.392	0	0	0	0	0
212			2	0.392	0	0	0	0	0
213			3	0.392	0	0	0	0	0
214			4	0.392	0	0	0	0	0
215			5	0.392	0	0	0	0	0
216	3	M6	1	0.392	0	0	0	0	0
217			2	0.392	0	0	0	0	0
218			3	0.392	0	0	0	0	0
219			4	0.392	0	0	0	0	0
220			5	0.392	0	0	0	0	0
221	3	M7	1	0.007	0	0	0	0	0
222			2	0.007	0	0	0	0	0
223			3	0.007	0	0	0	0	0
224			4	0.007	0	0	0	0	0
225			5	0.007	0	0	0	0	0
226	3	M8	1	-0.024	0	0	0	0	0
227			2	-0.024	0	0	0	0	0
228			3	-0.024	0	0	0	0	0
229			4	-0.024	0	0	0	0	0
230			5	-0.024	0	0	0	0	0
231	3	M10	1	-0.024	0	0	0	0	0
232			2	-0.024	0	0	0	0	0
233			3	-0.024	0	0	0	0	0
234		The state of the s	4	-0.024	0	0	0	0	0
235			5	-0.024	0	0	0	0	0
236	3	M11	1	0.007	0	0	0	0	0
237		14/11	2	0.007	0	0	0	0	0
238			3	0.007	0	0	0	0	0
239			4	0.007	0	0	0	0	0
240			5	0.007	0	0	0	0	0
241	3	M9	1	0.034	0	0	0	0	0
242	J	IVIO	2	0.034	0	0	0	0	0
242			3	0.034	0	0	0	0	0
244			4	0.034	0	0	0	0	0
244			4	0.034	U	<u> </u>	U	U	U



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M20 M20 M21	5 1 2 3 4 5 1 2 3 4 5	0.034 0.392 0.392 0.392 0.392 0.392 0.002 0.002	0 -0.007 -0.007 -0.007 -0.007 -0.007 0 0.005	0 0 0 0 0 0	0 0 0 0 0	0 0 0 0	0 0 0.017 0.033
M20	2 3 4 5 1 2 3 4 5	0.392 0.392 0.392 0.392 0 0.002 0.004	-0.007 -0.007 -0.007 -0.007 0 0.005	0 0 0 0	0 0 0	0	0.017 0.033
	3 4 5 1 2 3 4 5	0.392 0.392 0.392 0 0.002 0.004	-0.007 -0.007 -0.007 0 0.005	0 0 0 0	0	0	0.033
	4 5 1 2 3 4 5	0.392 0.392 0 0.002 0.004	-0.007 -0.007 0 0.005	0 0 0	0		
	5 1 2 3 4 5	0.392 0 0.002 0.004	-0.007 0 0.005	0		0	THE RESERVE AND ADDRESS OF THE PARTY OF THE
	1 2 3 4 5	0 0.002 0.004	0 0.005	0	0		0.05
	2 3 4 5	0.002 0.004	0.005		U	0	0.066
M21	3 4 5	0.004			0	0	0
M21	4 5			0	0	0	-0.002
M21	5	0.006	0.01	0	0	0	-0.006
M21		0.000	0.015	0	0	0	-0.014
M21		0.008	0.019	0	0	0	-0.025
	1	-0.091	-0.218	0	0	0	-0.025
	2	-0.089	-0.213	0	0	0	0.115
	3	-0.087	-0.209	0	0	0	0.252
	4	-0.085	-0.204	0	0	0	0.386
	5	-0.083	-0.199	0	0	0	0.517
M22	1	-0.445	-0.048	0	0	0	0.517
	2	-0.44	-0.036	0	0	0	0.583
	3	-0.435	-0.025	0	0	0	0.631
	4	-0.43	-0.013	0	0	0	0.661
	5	-0.425	-0.001	0	0	0	0.671
M23	1	-0.422	0.006	0	0	0	0.671
	2	-0.415	0.024	Ö	0	0	0.635
	3	-0.407	0.042	0	0	0	0.555
	4	-0.399	0.06	0	0	0	0.43
	5	-0.392	0.079	0	0	0	0.261
M24	1	-0.401	0.056	0	0	0	0.261
,,,,_,	2	-0.393	0.076	0	0	0	0.086
	3	-0.385	0.096	0	0	0	-0.14
	4	-0.377	0.115	0	0	0	-0.419
	5	-0.368	0.135	0	0	0	-0.749
M25	1	-0.368	-0.135	0	0	0	-0.749
WIE	2	-0.377	-0.115	0	0	0	-0.419
200 B 100 B	3	-0.385	-0.096	0	0	0	-0.14
was wall to come as	4	-0.393	-0.076	0	0	0	0.086
NAME OF THE OWNER O	5	-0.401	-0.056	0	0	0	0.261
M26	1	-0.392	-0.079	0	0	0	0.261
WIZO	2	-0.399	-0.06	0	0	0	0.43
	3	-0.407	-0.042	0	0	0	0.555
							0.635
				THE RESERVE AND ADDRESS OF THE PARTY OF THE			0.671
M27							0.671
IVIZI							0.661
							0.631
							0.583
							0.517
M28							0.517
IVIZU							0.386
							0.252
							0.252
							-0.025
							-0.025
M20							-0.025
M29							-0.014 -0.006
M29	3						-0.006
The state of the s	M27 M28 M29	M27 1 2 3 4 5 5 M28 1 2 3 3 4 4 5 5 M29 1 2 3 3	M27	4     -0.415     -0.024       5     -0.422     -0.006       M27     1     -0.425     0.001       2     -0.43     0.013       3     -0.435     0.025       4     -0.44     0.036       5     -0.445     0.048       M28     1     -0.083     0.199       2     -0.085     0.204       3     -0.087     0.209       4     -0.089     0.213       5     -0.091     0.218       M29     1     0.008     -0.019       2     0.006     -0.015       3     0.004     -0.01	4     -0.415     -0.024     0       5     -0.422     -0.006     0       M27     1     -0.425     0.001     0       2     -0.43     0.013     0       3     -0.435     0.025     0       4     -0.44     0.036     0       5     -0.445     0.048     0       M28     1     -0.083     0.199     0       2     -0.085     0.204     0       3     -0.087     0.209     0       4     -0.089     0.213     0       5     -0.091     0.218     0       M29     1     0.008     -0.019     0       M29     1     0.006     -0.015     0       3     0.004     -0.01     0	4       -0.415       -0.024       0       0         5       -0.422       -0.006       0       0         M27       1       -0.425       0.001       0       0         2       -0.43       0.013       0       0       0         3       -0.435       0.025       0       0       0         4       -0.44       0.036       0       0       0         5       -0.445       0.048       0       0       0         M28       1       -0.083       0.199       0       0         2       -0.085       0.204       0       0         3       -0.087       0.209       0       0         4       -0.089       0.213       0       0         5       -0.091       0.218       0       0         M29       1       0.008       -0.019       0       0         3       0.006       -0.015       0       0	4       -0.415       -0.024       0       0       0         5       -0.422       -0.006       0       0       0         M27       1       -0.425       0.001       0       0       0         2       -0.43       0.013       0       0       0         3       -0.435       0.025       0       0       0         4       -0.44       0.036       0       0       0         5       -0.445       0.048       0       0       0         M28       1       -0.083       0.199       0       0       0         2       -0.085       0.204       0       0       0       0         3       -0.087       0.209       0       0       0       0         4       -0.089       0.213       0       0       0       0         M29       1       0.008       -0.019       0       0       0       0         M29       1       0.006       -0.015       0       0       0       0



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	LC	Member Label	Sec	Axial[k]	y Shear[k]	z Shear[k]	Tor que[ k-ft]	y-y Moment[k-ft]	z-z Moment[k-ft]
300			5	0	0	0	0	0	0
301	3	M3	1	0.392	0.017	0	0	0	0.066
302			2	0.392	0.017	0	0	0	0.025
303			3	0.392	0.017	0	0	0	-0.016
304	Section Section		4	0.392	0.017	0	0	0	-0.057
305			5	0.392	0.017	0	0	0	-0.099
306	3	M4	1	0.392	-0.017	0	0	0	-0.099
307			2	0.392	-0.017	0	0	0	-0.057
308			3	0.392	-0.017	0	0	0	-0.016
309			4	0.392	-0.017	0	0	0	0.025
310			5	0.392	-0.017	0	0	0	0.066
311	3	M5	1	0.392	0.007	0	0	0	0.066
312			2	0.392	0.007	0	0	0	0.05
313			3	0.392	0.007	0	0	0	0.033
314			4	0.392	0.007	0	0	0	0.017
315			5	0.392	0.007	0	0	0	0
316	4	M1	1	-12.248	0	0	0	0	0
317			2	-12.248	0	0	0	0	0
318			3	-12.248	0	0	0	0	0
319			4	-12.248	0	0	0	0	0
320		The state of the s	5	-12.248	0	0	0	0	0
321	4	M6	1	-12.248	0	0	0	0	0
322			2	-12.248	0	0	0	0	0
323			3	-12.248	0	0	0	0	0
324			4	-12.248	0	0	0	0	0
325			5	-12.248	0	0	0	0	0
326	4	M7	11	-0.156	0	0	0	0	0
327			2	-0.156	0	0	0	0	0
328	900 March 2010	Market and the second second	3	-0.156	0	0	0	0	0
329			4	-0.156	0	0	0	0	0
330		rockers and a second second	5	-0.156	0	0	0	0	0
331	4	M8	1	0.79	0	0	0	0	0
332	Q1000000000000000000000000000000000000		2	0.79	0	0	0	0	0
333			3	0.79	0	0	0	0	0,
334			4	0.79	0	0	0	0	0
335			5	0.79	0	0	0	0	0
336	4	M10	1	0.79	0	0	0	0	0
337			2	0.79	0	0	0	0	0
338			3	0.79	0	0	0	0	0
339			4	0.79	0	0	0	0	0
340	Alberto e de la composition della composition de		5	0.79	0	0	0	0	0
341	4	M11	1	-0.156	0	0	0	0	0
342			2	-0.156	0	0	0	0	0
343			3	-0.156	0	0	0	0	0
344			4	-0.156	0	0	0	0	0
345		NAC	5	-0.156	0	0	0	0	0
346	4	M9	1	-1.109	0	0	0	0	0
347			2	-1.109	0	0	0	0	0
348			3	-1.109	0	0	0	0	0
349			4	-1.109	0	0	0	0	0
350	1	NAC	5	-1.109	0	0	0	0	0
351	4	M2	1	-12.247	0.231	0	0	0	0
352			2	-12.247	0.231	0	0	0	-0.519
353			3	-12.247	0.231	0	0	0	-1.038
354			4	-12.247	0.231	0	0	0	-1.557



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	LC	Member Label	Sec	Axial[k]	y Shear[k]	z Shear[k]	Tor que[k-ft]	y-y Moment[k-ft]	z-z Moment[k-ft]
355			5	-12.247	0.231	0	0	0	-2.075
356	4	M20	1	0	-0.001	0	0	0	0
357			2	-0.063	-0.153	0	0	0	0.05
358			3	-0.126	-0.304	0	0	0	0.199
359			4	-0.19	-0.456	0	0	0	0.446
360			5	-0.253	-0.608	0	0	0	0.791
361	4	M21	1	2.838	6.835	0	0	0	0.791
362			2	2.775	6.683	0	0	0	-3.602
363			3	2.711	6.532	0	0	0	-7.896
364			4	2.648	6.38	0	0	0	-12.092
365			5	2.585	6.229	0	0	0	-16.189
366	4	M22	1	13.86	1.506	0	0	0	-16.189
367			2	13.707	1.14	0	0	0	-18.268
368			3	13.554	0.774	0	0	0	-19.771
369			4	13.402	0.407	0	0	0	-20.699
370			5	13.249	0.041	0	0	0	-21.05
371	4	M23	1	13.188	-0.185	0	0	0	-21.05
372			2	12.951	-0.754	0	0	0	-19.907
373			3	12.714	-1.322	o l	Ö	0	-17.377
374			4	12.477	-1.891	0	0	0	-13.462
375			5	12.24	-2.459	Ō	Ō	0	-8.16
376	4	M24	1	12.546	-1.763	0	0	0	-8.16
377			2	12.289	-2.379	Ö	0	0	-2.692
378			3	12.032	-2.995	0	0	0	4.402
379			4	11.776	-3.61	0	0	0	13.123
380			5	11.519	-4.226	0	0	0	23.47
381	4	M25	1	11.519	4.226	Ö	0	0	23.47
382	•		2	11.776	3.61	0	0	0	13.123
383			3	12.032	2.995	0	0	0	4.402
384			4	12.289	2.379	0	0	0	-2.692
385			5	12.546	1.763	Ö	0	0	-8.16
386	4	M26	1	12.24	2.459	0	0	0	-8.16
387			2	12.477	1.891	o l	0	0	-13.462
388			3	12.714	1.322	0	0	0	-17.377
389			4	12.951	0.754	Ö	0	0	-19.907
390			5	13.188	0.185	0	0	0	-21.05
391	4	M27	1	13.249	-0.041	0	0	0	-21.05
392			2	13.402	-0.407	0	0	0	-20.699
393			3	13.554	-0.774	0	0	0	-19.771
394			4	13.707	-1.14	0	0	0	-18.268
395			5	13.86	-1.506	0	0	0	-16.189
396	4	M28	1	2.585	-6.229	0	0	0	-16.189
397			2	2.648	-6.38	0	0	0	-12.092
398			3	2.711	-6.532	0	0	0	-7.896
399			4	2.775	-6.683	0	0	0	-3.602
400			5	2.838	-6.835	0	0	0	0.791
401	4	M29	1	-0.253	0.608	Ö	0	0	0.791
402		20	2	-0.19	0.456	0	0	0	0.446
403			3	-0.126	0.304	0	0	0	0.199
404			4	-0.063	0.153	0	0	0	0.05
405			5	0.000	0.001	0	0	0	0.03
406	4	M3	1	-12.248	-0.529	0	0	0	-2.075
407		1410	2	-12.248	-0.529	0	0	0	-0.786
408			3	-12.248	-0.529	0	0	0	0.504
409			4	-12.248	-0.529	0	0	0	1.793



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	LC	Member Label	Sec	Axial[k]	y Shear[k]	z Shear[k]	Tor que[ k-ft]	y-y Moment[k-ft]	z-z Moment[k-ft]
410			5	-12.248	-0.529	0	0	0	3.083
411	4	M4	1	-12.248	0.529	0	0	0	3.083
412			2	-12.248	0.529	0	0	0	1.793
413			3	-12.248	0.529	0	0	0	0.504
414			4	-12.248	0.529	0	0	0	-0.786
415	1 1		5	-12.248	0.529	0	0	0	-2.075
416	4	M5	1	-12.247	-0.231	0	0	0	-2.075
417			2	-12.247	-0.231	0	0	0	-1.557
418			3	-12.247	-0.231	0	0	0	-1.038
419			4	-12.247	-0.231	0	0	0	-0.519
420			5	-12.247	-0.231	0	0	0	0.010
421	5	M1	1	-1.307	0	Ö	0	0	0
422	0	IVIII	2	-1.307	0	0	0	0	0
423			3	-1.307	0	0	0	0	0
424			4	-1.307	0	0			0
						THE RESERVE OF THE PARTY OF THE	0	0	
425		MC	5	-1.307	0	0	0	0	0
426	5	M6	1	-1.307	0	0	0	0	0
427			2	-1.307	0	0	0	0	0
428			3	-1.307	0	0	0	0	0
429			4	-1.307	0	0	0	0	0
430			5	-1.307	0	0	0	0	0
431	5	M7	1	-0.024	0	0	0	0	0
432			2	-0.024	0	0	0	0	0
433			3	-0.024	0	0	0	0	0
434			4	-0.024	0	0	0	0	0
435			5	-0.024	0	0	0	0	0
436	5	M8	1	0.081	0	0	0	0	0
437			2	0.081	0	0	0	0	0
438			3	0.081	0	0	0	0	0
439			4	0.081	0	0	0	0	Ö
440			5	0.081	0	0	0	0	0
441	5	M10	1	0.081	0	0	0	0	0
442			2	0.081	0	0	0	0	0
443			3	0.081	0	0	0	0	0
444			4	0.081	0	0	0	0	0
445			5	0.081	0	0	0	0	0
446	5	M11	1	-0.024	0	0	0	0	0
447	<u> </u>	IVITI	2	-0.024	0	0	0	0	0
448		Post continue de la c	3	-0.024	0	0	0		0
449			4	-0.024	0	THE RESERVE THE PARTY OF THE PA	0	0	
450					7	0		0	0
450	E	MO	5	-0.024	0	0	0	0	0
451	5	M9		-0.114	0	0	0	0	0
452			2	-0.114	0	0	0	0	0
453			3	-0.114	0	0	0	0	0
454			4	-0.114	0	0	0	0	0
455			5	-0.114	0	0	0	0	0
456	5	M2	1	-1.307	0.025	0	0	0	0
457			2	-1.307	0.025	0	0	0	-0.055
458			3	-1.307	0.025	0	0	0	-0.111
459			4	-1.307	0.025	0	0	0	-0.166
460			5	-1.307	0.025	0	0	0	-0.222
461	5	M20	1	0	0	0	0	0	0
462			2	-0.007	-0.016	0	0	0	0.005
463			3	-0.013	-0.032	0	0	0	0.021
464			4	-0.02	-0.049	0	0	0	0.047



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Checked By: JKF

	LC	Member Label	Sec	Axial[k]	y Shear[k]	z Shear[k]	Tor que[ k-ft]	y-y Moment[k-ft]	z-z Moment[k-ft]
465			5	-0.027	-0.065	0	0	0	0.084
466	5	M21	1	0.303	0.728	0	0	0	0.084
467			2	0.296	0.712	0	0	0	-0.384
468			3	0.29	0.696	0	0	0	-0.841
469			4	0.283	0.679	0	0	0	-1.288
470			5	0.276	0.663	0	0	0	-1.724
471	5	M22	1	1.482	0.16	0	0	0	-1.724
472			2	1.466	0.121	0	0	0	-1.945
473			3	1.449	0.082	0	0	0	-2.105
474			4	1.433	0.043	0	0	0	-2.203
475			5	1.417	0.004	0	0	0	-2.24
476	5	M23	1	1.408	-0.019	0	0	0	-2.24
477			2	1.382	-0.08	0	0	0	-2.119
478			3	1.357	-0.141	0	0	0	-1.851
479			4	1.332	-0.201	Ö	0	0	-1.434
480			5	1.306	-0.262	0	0	0	-0.869
481	5	M24	1	1.338	-0.187	0	0	0	-0.869
482		1121	2	1.31	-0.253	0	0	0	-0.288
483			3	1.283	-0.319	0	0	Ŏ	0.468
484			4	1.255	-0.385	0	0	0	1.397
485			5	1.228	-0.451	0	Ŏ	0	2.5
486	5	M25	1	1.228	0.451	0	0	0	2.5
487	<u> </u>	IVIZO	2	1.255	0.385	0	0	0	1.397
488			3	1.283	0.319	0	0	0	0.468
489			4	1.31	0.253	0	0	0	-0.288
490			5	1.338	0.233	0	0	0	-0.869
491	5	M26	1	1.306	0.167	0	0	0	-0.869
492	5	IVIZO	2	1.332	0.202	0	0		-1.434
				1.357				0	-1.851
493			3		0.141	0	0	0	
494			4	1.382	0.08	0	0	0	-2.119
495		N407	5	1.408	0.019	0	0	0	-2.24
496	5	M27	1	1.417	-0.004	0	0	0	-2.24
497			2	1.433	-0.043	0	0	0	-2.203
498			3	1.449	-0.082	0	0	0	-2.105
499			4	1.466	-0.121	0	0	0	-1.945
500		1400	5	1.482	-0.16	0	0	0	-1.724
501	5	M28	1	0.276	-0.663	0	0	0	-1.724
502			2	0.283	-0.679	0	0	0	-1.288
503		1	3	0.29	-0.696	0	0	0	-0.841
504		74.00	4	0.296	-0.712	0	0	0	-0.384
505	_	N400	5	0.303	-0.728	0	0	0	0.084
506	5	M29	1	-0.027	0.065	0	0	0	0.084
507			2	-0.02	0.049	0	0	0	0.047
508	Contraga de		3	-0.013	0.032	0	0	0	0.021
509			4	-0.007	0.016	0	0	0	0.005
510			5	0	0	0	0	0	0
511	5	M3	1	-1.307	-0.056	0	0	0	-0.222
512			2	-1.307	-0.056	0	0	0	-0.084
513			3	-1.307	-0.056	0	0	0	0.054
514			4	-1.307	-0.056	0	0	0	0.191
515			5	-1.307	-0.056	0	0	0	0.329
516	5	M4	1	-1.307	0.056	0	0	0	0.329
517			2	-1.307	0.056	0	0	0	0.191
518			3	-1.307	0.056	0	0	0	0.054
519			4	-1.307	0.056	0	0	0	-0.084



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	LC	Member Label	Sec	Axial[k]	y Shear[k]	z Shear[k]	Tor que[k-ft]	y-y Moment[k-ft]	z-z Moment[k-ft]
520			5	-1.307	0.056	0	0	0	-0.222
521	5	M5	1	-1.307	-0.025	0	0	0	-0.222
522			2	-1.307	-0.025	0	0	0	-0.166
523			3	-1.307	-0.025	0	0	0	-0.111
524			4	-1.307	-0.025	0	0	0	-0.055
525			5	-1.307	-0.025	0	0	0	0
526	6	M1	1	3.004	0	0	0	0	0
527			2	3.004	0	0	0	0	0
528			3	3.004	0	0	0	0	0
529			4	3.004	0	0	0	0	0
530			5	3.004	0	0	0	0	0
531	6	M6	1	3.004	0	0	0	0	0
532			2	3.004	0	0	0	0	0
533			3	3.004	0	0	0	0	0
534			4	3.004	0	0	0	0	0
535			5	3.004	0	0	Ō	0	0
536	6	M7	1	0.061	0	0	0	0	0
537			2	0.061	Ö	Ö	0	. 0	0
538			3	0.061	0	0	0	0	0
539			4	0.061	0	0	Ö	0	0
540			5	0.061	0	0	0	0	0
541	6	M8	1	-0.185	0	0	0	0	0
542		1110	2	-0.185	0	0	0	0	0
543			3	-0.185	Ö	0	0	0	0
544			4	-0.185	0	0	0	0	0
545			5	-0.185	0	0	0	0	0
546	6	M10	1	-0.185	0	0	0	0	0
547		WITO	2	-0.185	0	0	0	0	0
548			3	-0.185	0	0	0	0	0
549			4	-0.185	0	0	0	0	0
550			5	-0.185	0	0	0	0	0
551	6	M11	1	0.061	0	0	0	0	0
552	U	IVI I I	2	0.061	0			0	
553	4		3	0.061	THE RESIDENCE AND ADDRESS OF THE PARTY OF TH	0	0		0
554			4	0.061	0	0	0	0	0
555			5	0.061	0	0	0	0	0
556	6	M9	1	0.061		0	0	0	0
	6	IVIS			0	0	0	0	0
<b>557</b> 558			2	0.257	0	0	0	0	0
559			3	0.257	0	0	0	0	0
			4	0.257	0	0	0	0	0
560	6	MO	5	0.257	0	0	0	0	0
561	6	M2		3.004	-0.057	0	0	0	0 107
562			2	3.004	-0.057	0	0	0	0.127
563			3	3.004	-0.057	0	0	0	0.255
564			4	3.004	-0.057	0	0	0	0.382
565		MOO	5	3.004	-0.057	0	0	0	0.509
566	6	M20	1	0	0	0	0	0	0
567		V	2	0.016	0.037	0	0	0	-0.012
568			3	0.031	0.074	0	0	0	-0.048
569			4	0.047	0.112	0	0	0	-0.109
570			5	0.062	0.149	0	0	0	-0.194
571	6	M21	1	-0.697	-1.672	0	0	0	-0.194
572			2	-0.682	-1.635	0	0	0	0.881
573			3	-0.666	-1.598	0	0	0	1.931
574			4	-0.651	-1.56	0	0	0	2.958



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	LC	Member Label	Sec	Axial[k]	y Shear[k]	z Shear[k]	Tor que[k-ft]	y-y Moment[k-ft]	z-z Moment[k-ft]
575	1500		5	-0.635	-1.523	0	0	0	3.96
576	6	M22	1	-3.41	-0.368	0	0	0	3.96
577			2	-3.372	-0.278	0	0	0	4.468
578			3	-3.335	-0.188	0	0	0	4.834
579			4	-3.297	-0.098	0	0	0	5.059
580			5	-3.26	-0.008	0	0	0	5.143
581	6	M23	1	-3.236	0.043	0	0	0	5.143
582			2	-3.178	0.183	0	0	0	4.867
583			3	-3.12	0.323	0	0	0	4.251
584			4	-3.062	0.462	0	0	0	3.294
585			5	-3.003	0.602	0	0	0	1.996
586	6	M24	1	-3.074	0.43	0	0	0	1.996
587			2	-3.011	0.581	0	0	0	0.661
588			3	-2.948	0.733	0	0	0	-1.073
589			4	-2.885	0.884	0	0	0	-3.208
590			5	-2.822	1.035	0	0	0	-5.741
591	6	M25	1	-2.822	-1.035	0	0	0	-5.741
592			2	-2.885	-0.884	0	0	0	-3.208
593			3	-2.948	-0.733	0	Ŏ	0	-1.073
594			4	-3.011	-0.581	0	Ō	0	0.661
595			5	-3.074	-0.43	0	0	0	1.996
596	6	M26	1	-3.003	-0.602	0	0	0	1.996
597		1112	2	-3.062	-0.462	0	0	0	3.294
598			3	-3.12	-0.323	0	0	0	4.251
599			4	-3.178	-0.183	0	0	0	4.867
600			5	-3.236	-0.043	0	0	0	5.143
601	6	M27	1	-3.26	0.008	0	0	0	5.143
602		14121	2	-3.297	0.098	0	0	0	5.059
603			3	-3.335	0.188	0	0	0	4.834
604			4	-3.372	0.278	0	0	0	4.468
605			5	-3.41	0.368	0	0	0	3.96
606	6	M28	1	-0.635	1.523	0	0	0	3.96
607		WIZO	2	-0.651	1.56	0	0	0	2.958
608			3	-0.666	1.598	0	0	0	1.931
609			4	-0.682	1.635	0	0	0	0.881
610			5	-0.697	1.672	0	0	0	-0.194
611	6	M29	1	0.062	-0.149	0	0	0	-0.194
612	0	WIZO	2	0.047	-0.112	0	0	0	-0.109
613			3	0.031	-0.074	0	0	0	-0.048
614			4	0.016	-0.037	0	0	0	-0.012
615			5	0.010	0	0	0	0	0
616	6	M3	1	3.004	0.13	0	0	0	0.509
617	J	IVIO	2	3.004	0.13	0	0	0	0.193
618			3	3.004	0.13	0	0	0	-0.123
619			4	3.004	0.13	0	0	0	-0.123
620			5	3.004	0.13	0	0	0	-0.756
621	6	M4	1	3.004	-0.13	0	0	0	-0.756
622	U	TIVI	2	3.004	-0.13	0	0	0	-0.730
623			3	3.004	-0.13	0	0	0	-0.123
624			4	3.004	-0.13	0	0	0	0.193
625			5	3.004	-0.13	0	0	0	0.509
626	6	M5	1	3.004	0.057	0	0	0	0.509
627	U	IVIO	2	3.004	0.057	0	0	0	0.382
628			3	3.004	0.057		0		0.255
629						0		0	
029			4	3.004	0.057	0	0	0	0.127



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	LC	Member Label	Sec	Axial[k]	y Shear[k]	z Shear[k]	Tor que[k-ft]	y-y Moment[k-ft]	z-z Moment[k-ft]
630	LU	Meninei Fanel	5	3.004	0.057	0	0	y-y womentik-itj	0
331	7	M1	1	-18.775	0.037	0	0	0	0
332	1	IVI I	2	-18.775	0	0	0	0	0
333			3	-18.775	0	0	0	0	0
334			4	-18.775	0	0	0	0	0
635			5	-18.775	0	0	0	0	0
636	7	M6	1	-18.775	0	0	0	0	0
637		IVIO	2	-18.775	0	0	0	0	0
638			3	-18.775	0	0	0	0	0
639			4	-18.775	0	0	0	0	0
640			5	-18.775	0	0	0	0	0
641	7	M7	1	-0.177	0	0	0	0	0
642		1017	2	-0.177	0	0	0	0	0
643			3	-0.177	0	0	0	0	0
644			4	-0.177	0	0	0	0	0
645			5	-0.177	0	0	0	0	0
646	7	M8	1	1.237	0	0	0	0	0
647		IVIO	2	1.237	0	0	0	0	0
648	ACTION OF THE		3	1.237	0	0	0	0	0
649			4	1.237	0	0	0	0	0
650			5	1.237	0	0	0	0	0
651	7	M10	1	1.237	0	0	0	0	0
652	SEPTEMBER STATE		2	1.237	0	0	0	0	0
653			3	1.237	0	Ö	Ö	0	0
654			4	1.237	0	0	0	0	0
655			5	1.237	0	0	0	0	0
656	7	M11	1	-0.177	0	0	0	0	0
657		100	2	-0.177	Ö	0	Ŏ	0	0
658			3	-0.177	0	0	0	0	0
659			4	-0.177	Ō	0	Ō	0	0
660			5	-0.177	0	0	0	0	0
661	7	M9	1	-1.743	0	Ō	Ō	Ō	0
662			2	-1.743	0	0	0	0	0
663			3	-1.743	0	0	0	0	0
664			4	-1.743	0	0	0	0	0
665			5	-1.743	0	0	0	0	0
666	7	M2	1	-18.773	0.353	0	0	0	0
667			2	-18.773	0.353	0	0	0	-0.795
668			3	-18.773	0.353	0	0	0	-1.59
669		(1) 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	4	-18.773	0.353	0	0	0	-2.385
670			5	-18.773	0.353	0	0	0	-3.181
671	7	M20	1	0	-0.003	0	0	0	0
672			2	-0.097	-0.235	0	0	0	0.077
673			3	-0.193	-0.467	0	0	0	0.306
674			4	-0.29	-0.699	0	0	0	0.685
675			5	-0.387	-0.932	0	0	0	1.215
676	7	M21	1	4.346	10.49	0	0	0	1.215
677			2	4.249	10.258	0	0	0	-5.527
678			3	4.153	10.025	0	0	0	-12.118
679			4	4.056	9.793	0	0	0	-18.559
680			5	3.959	9.561	0	0	0	-24.848
681	7	M22	1	21.217	2.312	0	0	0	-24.848
682			2	20.983	1.751	0	0	0	-28.04
683			3	20.749	1.19	0	0	0	-30.35
684			4	20.515	0.629	0	0	0	-31.778



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	LC	Member Label	Sec	Axial[k]	y Shear[k]	z Shear[k]	Tor que[k-ft]	y-y Moment[k-ft]	z-z Moment[k-ft]
685			5	20.282	0.068	0	0	0	-32.325
686	7	M23	1	20.212	-0.289	0	0	0	-32.325
687			2	19.849	-1.16	0	0	0	-30.559
388			3	19.486	-2.031	0	0	0	-26.67
389			4	19.124	-2.901	0	0	0	-20.659
690			5	18.761	-3.772	0	0	0	-12.525
691	7	M24	1	19.24	-2.71	0	0	0	-12.525
692			2	18.847	-3.653	0	0	0	-4.125
693			3	18.454	-4.596	0	0	0	6.766
694			4	18.061	-5.539	0	0	0	20.149
695			5	17.668	-6.483	0	0	0	36.022
396	7	M25	1	17.668	6.483	0	0	0	36.022
697			2	18.061	5.539	0	0	0	20.149
698			3	18.454	4.596	0	0	0	6.766
699			4	18.847	3.653	0	0	0	-4.125
700			5	19.24	2.71	0	0	0	-12.525
701	7	M26	1	18.761	3.772	0	0	0	-12.525
702			2	19.124	2.901	0	0	0	-20.659
703			3	19.486	2.031	0	0	0	-26.67
704			4	19.849	1.16	0	0	0	-30.559
705			5	20.212	0.289	0	0	0	-32.325
706	7	M27	1	20.282	-0.068	0	0	0	-32.325
707			2	20.515	-0.629	0	0	0	-31.778
708			3	20.749	-1.19	0	0	0	-30.35
709			4	20.983	-1.751	0	0	0	-28.04
710			5	21.217	-2.312	0	0	0	-24.848
711	7	M28	1	3.959	-9.561	0	0	0	-24.848
712			2	4.056	-9.793	0	0	0	-18.559
713			3	4.153	-10.025	0	0	0	-12.118
714			4	4.249	-10.258	0	0	0	-5.527
715			5	4.346	-10.49	0	0	0	1.215
716	7	M29	1	-0.387	0.932	0	0	0	1.215
717			2	-0.29	0.699	Ö	0	0	0.685
718			3	-0.193	0.467	0	0	0	0.306
719			4	-0.097	0.235	Ö	0	0	0.077
720			5	0	0.003	0	0	0	0
721	7	M3	1	-18.777	-0.811	0	0	0	-3.181
722			2	-18.777	-0.811	0	0	0	-1.204
723			3	-18.777	-0.811	0	0	0	0.773
724			4	-18.777	-0.811	0	0	0	2.749
725			5	-18.777	-0.811	0	0	0	4.726
726	7	M4	1	-18.777	0.811	0	0	0	4.726
727			2	-18.777	0.811	0	0	0	2.749
728			3	-18.777	0.811	0	0	0	0.773
729			4	-18.777	0.811	0	0	0	-1.204
730			5	-18.777	0.811	0	0	0	-3.181
731	7	M5	1	-18.773	-0.353	0	0	0	-3.181
732			2	-18.773	-0.353	0	0	0	-2.385
733			3	-18.773	-0.353	0	0	0	-1.59
734			4	-18.773	-0.353	0	0	0	-0.795
735			5	-18.773	-0.353	0	0	0	0



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### Maximum Member Section Forces

Legisland			minum mombo												
1   1   M1		LC	Member Labe	l Axial[	k]Loc[ft]	y Shear[k	]Loc[ft]	z Shear[k	[Loc[ft]	Tor que[k-	ft]Loc[ft]	y-y Moment[k-ft	]Loc[ft]	z-z Moment[k-	ft]Loc[ft]
2	1	1	M1							THE RESIDENCE NAME AND ADDRESS OF					
3	2					0									
4	10717200000000	1	M6	TWO CONTRACTOR OF THE PROPERTY	And the result of the con-	production and an arrangement		CONTRACTOR CONTRACTOR		BATTER OF THE STATE OF THE STAT				Particular and the second seco	
S		1000	IVIO		_										
6	_	1	N/17			STATE OF THE PARTY		CONTRACTOR STATE		ALL PARTY OF THE P			-		_
Total   MB		1	IVI /							and the same of th					
8	1707 ST 4075450		140	WINDSON, CARL STONE AND ADDRESS.	THE RESERVED AND ADDRESS.	District Colon State Sta		TOTAL STREET,		Control of the Control				CONTRACTOR STATE OF THE PARTY O	
9   1	TAXABLE PARTY	1	NI8							Participation of the Participa			6.167		6.167
10	Contract to the second	Table Service		A STATE OF THE PARTY OF THE PAR		PRINCIPLE STATE OF THE	_			Wall and Applications of the Park		0		0	
11		1	M10			0	6.167	0	6.167	0	6.167	0	6.167	0	6.167
12	10			min 0.414	0	0	0	0	0	0	0	0	0	0	0
12	11	1	M11	max -0.10	2 2.417	0	2.417	0	2.417	0	2.417	0	2.417	0	2.417
13	12			min -0.10	2 0	0	0	0	0	0	0	0		0	
14	13	1	M9	max -0.58	10.23	0	10 23	0	10 23	0		No. 1015 Williams Control of the Con		AND DESCRIPTION OF PERSONS ASSESSMENT OF THE	and the second s
15		973													
16		1	M2	The second second second				THE RESERVE OF THE PERSON NAMED IN	W. C.	Water to Product and the	CONTRACT OF CONTRA		500 TOHEROY 2 & 227		SOUR MANAGEMENT HAVE
17		1924	IVIZ				NAME OF TAXABLE PARTY.		-						
18		1	MOO	Elizabeth Strainst Accorden	SAME SAME DOWN AND ADDRESS OF THE PARTY NAMED IN	CONTRACTOR AND ADDRESS OF THE PARTY OF THE P	20000000000000000000000000000000000000	The state of the s		THE RESERVE OF THE PERSON NAMED IN COLUMN 1					
19   1			IVIZU		The Person Person		-	CONTRACTOR OF THE PARTY OF THE							
Description   Description		15000000				MANUFACTURE OF THE PARTY OF THE	A HARRY MARKS STREET	THE RESIDENCE OF THE PARTY OF T	The state of the s	Marie Company of the					COMP. STREET,
1		1	M21				-		2.6	0	2.6	0	2.6		0
22							2.6	0	0	0		0	0	-8.634	2.6
23		1	M22	max 7.408	0	0.803	0	0	6.284	0	6.284	0	6.284	-8.634	0
23   1   M23	22			min 7.082	6.284	0.02	6.284	0	0	0	0	0			6.284
24	23	1	M23	max 7.042	2 0	-0.097	THE RESERVE OF THE PARTY OF THE	0	9.75	0					CARL SQUARESTANDONNA
25															
26		1	M24	CONTRACTOR	COLUMN TO THE PARTY OF THE PART		PERSONAL PROPERTY OF THE PARTY	SURFACE DOWNSTRATED TO SERVICE STATES		CONTRACTOR SOMETHING					Total Commission of the last
27			1412-1				-		100 Nanahananak			and the second s			
28		1	M25	sub-triouse straight and strains			THE RESIDENCE OF THE PERSON NAMED IN COLUMN 1		-	SALES OF THE SALES OF THE SALES	_	Control of the Contro	Total Control of the last of t		CONT. CONT. CO. CO. CO. CO. CO. CO. CO. CO. CO. CO
29			IVIZO												NAME OF TAXABLE PARTY OF TAXABLE PARTY.
30			1400		The second second second second second			AND DESCRIPTION OF THE PARTY OF			_				CHILD CONTROL CONTROL
31   1   M27   max   7.408   6.284   -0.02   0   0   6.284   0   6.284   0   6.284   0   6.284   32   min   7.082   0   -0.803   6.284   0   0   0   0   0   0   0   0   0		1	M26				THE PERSON NAMED IN						9.75		
32		Marie Cons		PROPERTY AND ADDRESS OF THE PARTY OF THE PAR	CO. SEPTEMBER SERVICES.		9.75	0		0		0			9.75
33   1   M28   max   1.516   2.6   -3.322   0   0   2.6   0   2.6   0   2.6   0   0   2.6   0   0   0   0   0   0   0   0   3.634   0   0   3.645   2.6   0   0   0   0   0   0   0   0   0		1	M27				The second second	0	6.284	0	6.284	0	6.284	-8.634	6.284
34				min 7.082	0	-0.803	6.284	0	0	0	0	0	0	-11.222	0
34	33	1	M28	max 1.516	2.6	-3.322	0	0	2.6	0	2.6	0	2.6	0.422	2.6
35   1   M29   max   0   2.6   0.324   0   0   2.6   0   0   0   0   0   0   0   0   0	34			min 1.381	0	-3.645	2.6	0	0	0		0		-8.634	
36	35	1	M29	Decreased the street of the st			THE RESERVE THE PARTY OF THE PA	0	26	0		And the second s			SCAN SERVICE STREET, S
37         1         M3         max -6.539         9.75         -0.282         9.75         0         9.75         0         9.75         1.646         9.75           38         min -6.539         0         -0.282         0         0         0         0         0         0         -1.108         0           39         1         M4         max -6.539         9.75         0.282         9.75         0         9.75         0         9.75         1.646         0           40         min -6.539         0         0.282         0         0         0         0         0         0         -1.108         9.75           41         1         M5         max -6.538         9         -0.123         9         0 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td>26</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>							26								
38		1	M3			THE RESERVE AND ADDRESS OF THE PARTY OF THE		ANALYSIS STREET, STREE		AL ARTHUR VIOLENCE AND ADDRESS OF THE PARTY					CANCEL SPECIAL CONTRACTOR OF THE PARTY OF TH
39         1         M4         max -6.539         9.75         0.282         9.75         0         9.75         0         9.75         1.646         0           40         min -6.539         0         0.282         0         0         0         0         0         0         -1.108         9.75           41         1         M5         max -6.538         9         -0.123         9         0         9         0         9         0         9           42         min -6.538         0         -0.123         0         0         0         0         0         0         0         -1.108         0           43         2         M1         max-17.462         5.8         0         5.		335 1 (82)	IVIO												
40         min -6.539         0         0.282         0         0         0         0         0         0         -1.108         9.75           41         1         M5         max -6.538         9         -0.123         9         0         9         0         9         0         9           42         min -6.538         0         -0.123         0         0         0         0         0         0         -1.108         0           43         2         M1         max -17.462         5.8         0         <		1	NAA					THE RESERVE THE PERSON NAMED IN COLUMN 1		1107010-000-000-000-000-000-000-					Marie Company of the
41         1         M5         max -6.538         9         -0.123         9         0         0		16180	1014												
42         min -6.538         0 -0.123         0 0 0 0 0 0 0 0 0 -1.108         0           43         2 M1 max -17.462         5.8 0 5.8	TAX DESCRIPTION OF THE PARTY OF	1	D.C.				Transmitted to the second	The second second second		TANKS OF THE OWNER, WHEN THE PARTY OF THE PA	The state of the s	A Secretary of the Control of the Co		BURNESS BOOK AND STONE S	COLUMN TO SERVICE STREET, STRE
43         2         M1         max-17.462         5.8         0         5.8         0         5.8         0         5.8         0         5.8         0         5.8         0         5.8         0 </td <td></td> <td></td> <td></td> <td>max -6.538</td> <td>9</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>0</td> <td></td> <td></td> <td></td>				max -6.538	9							0			
44         min -17.462 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		10210		min -6.538	3 0			APPENDING TO THE PERSON NAMED AND ADDRESS OF THE PERSON NAMED ADDRESS OF THE PERSON NAMED AND							
45         2         M6         max-17.462         5.8         0         0		2	M1			0	5.8	0		0	5.8	0	5.8	0	5.8
45         2         M6         max-17.462         5.8         0         0	_					0		0	0	0	0	0	0	0	
46         min -17.462         0 <t< td=""><td>45</td><td>2</td><td>M6</td><td>max-17.46</td><td>2 5.8</td><td>0</td><td>5.8</td><td>0</td><td>5.8</td><td>0</td><td>5.8</td><td></td><td></td><td>0</td><td></td></t<>	45	2	M6	max-17.46	2 5.8	0	5.8	0	5.8	0	5.8			0	
47         2         M7         max -0.176 2.417         0         0         0						0									
48         min -0.176         0 <td< td=""><td></td><td>2</td><td>M7</td><td></td><td></td><td>State Control of Control of Control</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>		2	M7			State Control of Control of Control									
49         2         M8         max 1.146 6.167         0         6.167         0         6.167         0         6.167         0         6.167         0         6.167         0         6.167         0         6.167         0         6.167         0 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>															
50         min         1.146         0<		2	MA			MARKET CONTRACTOR OF THE PARTY			-	are control of the latest and the					
51         2         M10         max         1.146         6.167         0         6.167         0         6.167         0         6.167         0         6.167         0         6.167         0         6.167         0         6.167         0         6.167         0         6.167         0 <t< td=""><td></td><td>_</td><td>IVIO</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>		_	IVIO												
52         min         1.146         0<		2	MAC							MINISTER AND ADDRESS OF THE PARTY OF THE PAR	_				
53         2         M11         max -0.176         2.417         0         2.417         0         2.417         0         2.417         0         2.417         0         2.417         0         2.417         0		2	IVITU												
54 min -0.176 0 0 0 0 0 0 0 0 0 0 0		_													
		2	M11						2.417		2.417				2.417
55   2   M9  max -1.613   10.23   0   10.23   0   10.23   0   10.23   0   10.23   0   10.23			AND DESIGNATION OF THE PARTY OF			0				0				0	
	55	2	M9	max -1.613	10.23	0	10.23	0	10.23	0	10.23	0	10.23	0	10.23



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Checked By: JKF

	LC	Member Labe	el	Axial[k]	Loc[ft]	v Shear[k	1Loc[ft]	z Shear[k]	Loc[ft]	Tor quel k-ft	lLoc[ft]	y-y Moment[k-t	ft]Loc[ft]	z-z Moment[k-	ft]Loc[ft]
56				-1.613	0	0	0	0	0	0	0	0	0	0	0
57	2	M2	-	-17.461	9	0.329	9	0	9	0	9	0	9	0	0
58				-17.461	0	0.329	0	0	0	0	0	0	0	-2.958	9
59	2	M20	max	TOWNS AND SOME RESIDENCE	0	-0.002	0	0	2.6	0	2.6	0	2.6	1.13	2.6
60			min	-0.36	2.6	-0.866	2.6	0	0	0	0	0	0	0	0
61	2	M21	Ser State of Section 1	4.043	0	9.754	0	0	2.6	0	2.6	0	2.6	1.13	0
62				3.683	2.6	8.89	2.6	0	0	0	0	0	0	-23.105	2.6
63	2	M22		19.739		2.15	0	0	6.284	0	6.284	Ö	6.284	-23.105	0
64				18.869		0.062	6.284	0	0	0	0	0	0	-30.054	6.284
65	2	M23	THE RESERVE THE PERSON NAMED IN	18.799	100 to 10	-0.268	0	0	9.75	0	9.75	0	9.75	-11.647	9.75
66				17.449		-3.508	9.75	0	0	0	0	0	0	-30.054	0
67	2	M24		17.893	0	-2.519	0	0	10.563	Ö	10.563	0	10.563	33.495	10.563
68			_	16.43	10.563	-6.029	10.563		0	0	0	0	0	-11.647	0
69	2	M25		17.893			0	0	10.563	Ō	10.563	0	10.563	33.495	0
70				16.43	0	2.519	10.563	0	0	0	0	0	0	-11.647	10.563
71	2	M26	max	18.799	9.75	3.508	0	0	9.75	0	9.75	0	9.75	-11.647	0
72				17,449	0	0.268	9.75	0	0	0	0	0	0	-30.054	9.75
73	2	M27	max	19.739	6.284	-0.062	0	0	6.284	0	6.284	0	6.284	-23.105	6.284
74				18.869	0	-2.15	6.284	0	0	0	0	0	0	-30.054	0
75	2	M28		4.043	2.6	-8.89	0	0	2.6	0	2.6	Ō	2.6	1.13	2.6
76				3.683	0	-9.754	2.6	0	0	0	0	0	0	-23.105	0
77	2	M29	max	121/04/02/02/07/07/07/08/07/07/08	2.6	0.866	0	0	2.6	0	2.6	0	2.6	1.13	0
78			min	-0.36	0	0.002	2.6	0	0	0	0	0	0	0	2.6
79	2	M3	max	-17.464	9.75	-0.754	9.75	0	9.75	0	9.75	0	9.75	4.395	9.75
80				-17.464	0	-0.754	0	0	0	0	0	0	0	-2.958	0
81	2	M4	max	-17.464	9.75	0.754	9.75	0	9.75	0	9.75	0	9.75	4.395	0
82				-17.464	0	0.754	0	0	0	. 0	0	0	0	-2.958	9.75
83	2	M5	max	-17.461	9	-0.329	9	0	9	0	9	0	9	0	9
84			min	-17.461	0	-0.329	0	0	0	0	0	0	0	-2.958	0
85	3	M1	max	0.392	5.8	0	5.8	0	5.8	0	5.8	0	5.8	0	5.8
86			min	0.392	0	0	0	0	0	0	0	0	0	0	0
87	3	M6	max	0.392	5.8	0	5.8	0	5.8	0	5.8	0	5.8	0	5.8
88			min	0.392	0	0	0	0	0	0	0	0	0	0	0
89	3	M7	max	0.007	2.417	0	2.417	0	2.417	0	2.417	0	2.417	0	2.417
90			min		0	0	0	0	0	0	0	0	0	0	0
91	3	M8	max	-0.024	6.167	0	6.167	0	6.167	0	6.167	0	6.167	0	6.167
92				-0.024	0	0	0	0	0	0	0	0	0	0	0
93	3	M10	max	-0.024	6.167	0	6.167	0	6.167	0	6.167	0	6.167	0	6.167
94			min		0	0	0	0	0	0	0	0	0	0	0
95	3	M11		0.007		0	2.417		2.417	0	2.417	0	2.417	0	2.417
96				0.007	0	0	0	0	0	00	0	0	0	0	0
97	3	M9		0.034	10.23	0	10.23		10.23	0	10.23	0	10.23	0	10.23
98				0.034	0	0	0	0	0	0	0	0	0	0	0
99		M2		0.392	9	-0.007	9	0	9	0	9	0	9	0.066	9
100				0.392	0	-0.007	0	0	0	0	0	0	0	0	0
101	3	M20		0.008	2.6	0.019	2.6	0	2.6	0	2.6	0	2.6	0	0
102				0	0	0	0	0	0	00	0	0	0	-0.025	2.6
103	3	M21		-0.083		-0.199	2.6	0	2.6	0	2.6	0	2.6	0.517	2.6
104				-0.091	0	-0.218	0	0	0	0	0	0	0	-0.025	0
105		M22		-0.425			6.284		6.284	0	6.284	0	6.284	0.671	6.284
106				-0.445	0	-0.048	0	0	0	0	0	0	0	0.517	0
107		M23		-0.392		0.079	9.75	0	9.75	0	9.75	0	9.75	0.671	0
108				-0.422	0	0.006	0	0	0	0	0	0	0	0.261	9.75
109		M24		-0.368			10.563		10.563	0	10.563	0	10.563	0.261	0
110		W. Charles	min	-0.401	0	0.056	0	0	0	0	0	0	0	-0.749	10.563



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	LC	Member Labe	el	Axial[k]	Loc[ft]	v Shearſk	ll oc[ft]	z Shear[k	al ociffi	Tor quel k-ff	tll ociftly	-v Moment[k-f	tll ocifti	z-z Moment[k-	ff]] oc[ff]
111	3	M25	172 122 22 22 23 23 23 23	-0.368	0	-0.056	10.563	0	10.563		10.563	0	10.563	0.261	10.563
112		0	_	-0.401	200 00000000000000000000000000000000000		0	0	0	0	0	0	0	-0.749	0
113	3	M26		-0.392	0	-0.006	9.75	0	9.75	0	9.75	Ö	9.75	0.671	9.75
114				-0.422	9.75	-0.079	0	0	0	0	0	0	0	0.261	0
115	3	M27	max	DIMESTRA CUITOR	0	0.048	6.284	0	6.284	0	6.284	0	6.284	0.671	0
116	7		_	-0.445	6.284	0.001	0	0	0	0	0	0	0	0.517	6.284
117	3	M28		-0.083	0	0.218	2.6	0	2.6	0	2.6	0	2.6	0.517	0
118				-0.091	2.6	0.199	0	0	0	0	0	0	0	-0.025	2.6
119	3	M29	max	0.008	0	0	2.6	0	2.6	0	2.6	0	2.6	0	2.6
120			min	0	2.6	-0.019	0	0	0	0	0	0	0	-0.025	0
121	3	M3	max	0.392	9.75	0.017	9.75	0	9.75	0	9.75	0	9.75	0.066	0
122			min		0	0.017	0	0	0	0	0	0	0	-0.099	9.75
123	3	M4	max	0.392	9.75	-0.017	9.75	0	9.75	0	9.75	0	9.75	0.066	9.75
124			min		0	-0.017	0	0	0	0	0	0	0	-0.099	0
125	3	M5		0.392	9	0.007	9	0	9	0	9	0	9	0.066	0
126			min	TO CARRY OF THE PROPERTY OF THE PARTY OF THE	0	0.007	0	0	0	0	0	0	0	0	9
127	4	M1	max	-12.248	5.8	0	5.8	0	5.8	0	5.8	0	5.8	0	5.8
128				-12.248		0	0	0	0	0	0	0	0	0	0
129	4	M6	max	-12.248	5.8	0	5.8	0	5.8	Ō	5.8	0	5.8	Ö	5.8
130				-12.248		0	0	0	0	0	0	0	0	0	0
131	4	M7	max	-0.156	2.417	0	2.417	0	2.417	0	2.417	0	2.417	Ö	2.417
132			min	-0.156	0	0	0	0	0	0	0	0	0	0	0
133	4	M8	max	0.79	6.167	0	6.167	0	6.167	0	6.167	Ō	6.167	0	6.167
134			min	0.79	0	0	0	0	0	0	0	0	0	0	0
135	4	M10	max	0.79	6.167	0	6.167	0	6.167	0	6.167	0	6.167	0	6.167
136			min	0.79	0	0	0	0	0	0	0	0	0	0	0
137	4	M11	max	-0.156	2.417	0	2.417	0	2.417	0	2.417	Ō	2.417	0	2.417
138			min	-0.156	0	0	0	0	0	0	0	0	0	0	0
139	4	M9	max	-1.109	10.23	0	10.23	0	10.23	0	10.23	0	10.23	0	10.23
140			min	-1.109	0	0	0	0	0	0	0	0	0	0	0
141	4	M2	max	-12.247	9	0.231	9	0	9	0	9	0	9	0	0
142			min	-12.247	0	0.231	0	0	0	0	0	0	0	-2.075	9
143	4	M20	max	0	0	-0.001	0	0	2.6	0	2.6	0	2.6	0.791	2.6
144				-0.253	2.6	-0.608	2.6	0	0	0	0	0	0	0	0
145	4	M21		2.838	0	6.835	0	0	2.6	0	2.6	0	2.6	0.791	0
146			min	2.585	2.6	6.229	2.6	0	0	0	0	0	0	-16.189	2.6
147	4	M22		13.86	0	1.506	0	0	6.284	0	6.284	0	6.284	-16.189	0
148				13.249		0.041	6.284	0	0	0	0	0	0	-21.05	6.284
149	4	M23	max	13.188	0	-0.185	0	0	9.75	0	9.75	0	9.75	-8.16	9.75
150				12.24	9.75	-2.459	9.75	0	0	0	0	0	0	-21.05	0
151	4	M24		12.546		-1.763	0	0	10.563	0	10.563	0	10.563	23.47	10.563
152				11.519			10.563	0	0	0	0	0	0	-8.16	0
153	4	M25		12.546			0	0	10.563	0	10.563	0	10.563	23.47	0
154				11.519			10.563	0	0	0	0	0	0	-8.16	10.563
155	4	M26		13.188		2.459	0	0	9.75	0	9.75	0	9.75	-8.16	0
156				12.24		0.185	9.75	0	0	0	0	0	0	-21.05	9.75
157	4	M27		13.86		-0.041	0	0	6.284	0	6.284	0	6.284	-16.189	6.284
158				13.249			6.284	0	0	0	0	0	0	-21.05	0
159	4	M28		2.838	2.6	-6.229	0	0	2.6	0	2.6	0	2.6	0.791	2.6
160	ALL SALES		- TOOR LINE WAS I	2.585	0	-6.835	2.6	0	0	0	0	0	0	-16.189	0
161	4	M29		0	2.6	0.608	0	0	2.6	0	2.6	0	2.6	0.791	0
162				-0.253		0.001	2.6	0	0	0	0	0	0	0	2.6
163	4	M3		-12.248		-0.529	9.75	0	9.75	0	9.75	0	9.75	3.083	9.75
164				-12.248		-0.529	0	0	0	0	0	0	0	-2.075	0
165	4	M4	max	-12.248	9.75	0.529	9.75	0	9.75	0	9.75	. 0	9.75	3.083	0



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Color   Colo					CUCITI											
167   4		LC	Member Labe		Axial[k]	Loc[ft]	y Shear[k	]Loc[ft]	z Shear[k]	Loc[ft]	Tor que[k-ft]	]Loc[ft]	y-y Moment[k-f	t]Loc[ft]	z-z Moment[k-	ft]Loc[ft]
167   4	166			min	-12.248	0	0.529	0	0	0	0	0	0	0	-2.075	9.75
188		4	M5	max	-12.247	9	-0.231	9	0	9	0	9	0	9	China College College College State Schools of State	CHARLEST CONTRACTOR
169   5		20.0074						-				-			-2 075	
170		5	M1		A. C.		Name of the Owner, with the	The state of the s			AMERICAN CONTRACTOR AND ADDRESS OF THE PARTY	THE RESERVE OF THE PERSON NAMED IN				
171   6		J	IVIII								ATT THE PARTY OF T					
172	ACCORDING TO A SEC.	F	NAC			THE RESERVE TO A STREET THE PARTY OF THE PAR	SHEET SHEETING TO BE SHEET	THE RESERVE THE PARTY OF THE PA		Total Control of the	Personal State Company of Company					
173   6		5	IVIO													
174				T 02 1/10 (F01)	SATURDAY CONTRACTOR	NUMBER OF STREET	STATE OF THE PARTY OF THE PARTY.	The second desired to	ACCOUNT OF A CONTRACTOR	100131004032003400	NAME OF TAXABLE PARTY.					
175   5	173	5	M7	max	-0.024	2.417	0	2.417	0	2.417	0	2.417	0	2.417	0	2.417
1776	174			min	-0.024	0	0	0	0	0	0	0	0	0	0	0
177   5	175	5	M8	max	0.081	6.167	0	6.167	0	6.167	0	6.167	0	6.167	0	6.167
178	176			min	0.081	0	0	0	0	0	0	0	0	0	0	0
178	177	5	M10	max	0.081	6.167	0	6.167	0	6.167	0	6.167	0	6.167	0	6.167
179   5												1000	140-140-140-140-140-140-140-140-140-140-		The Part of the Pa	1
180	THE RESERVE AND PARTY AND PARTY.	5	M11	S SECTION AND ADDRESS.	THICKNESS CONTRACTOR	The Real Property lies and the least lies and the lies and the lies and the least lies and the least lies and the lies and t			Control of the Contro		CONTRACTOR OF THE PARTY OF THE				THE RESIDENCE OF THE PARTY OF T	Marin Charles to Audit Marin Control
181   5   M9		J	IVIII			_				THE REAL PROPERTY.	No. 20100 10000 - Contract 10000		AND DESCRIPTION OF THE PARTY OF			
183   5	-	F	NAO	C. Berlinson Roses,	TALK WAS ASSESSED.	M2000000000000000000000000000000000000	THE RESERVE OF THE PARTY OF THE		EXCLUSION CONTRACTOR CONTRACTOR		The second secon	THE PERSON NAMED IN COLUMN	A A VANA SER SEASON SERVICE SE	AND RESIDENCE OF THE PARTY OF T		
183   5		0	IVI9				The state of the s								A STATE OF THE PARTY OF THE PAR	
184	TOTAL STREET, STREET, ST.				THE R. P. LEWIS CO., LANSING, Vol. 2, 1804.	SEASON STATES		NAME OF TAXABLE PARTY.	RUMAN SHOULD STREET AND AD	PARTY PROPERTY OF	Charles and the Control of the Control	H 140/2007/00/00/00/24/00/00		TO STATE OF STREET		TAKE SENANDAN PARA
185         5         M20         max         0         0         0         0         2.6         0         2.6         0.084         2.6           186         min         0.027         2.6         -0.065         2.6         0		5	M2			9		9	0	9	0		0	9	The state of the s	
186				min	-1.307	0	0.025	0	0		0		0			
187   5   M21   max   0.303   0   0.728   0   0   2.6   0   2.6   0   0.084   0     188   5   M22   max   1.482   0   0.16   0   0   0.284   0   0.284   0   0.284   1.724   0.094     190   min   1.417   6.284   0.004   6.284   0   0   0   0   0   0   0   0   0     191   5   M23   max   1.408   0   0.019   0   0   0   0   0   0   0   0   0	185	5	M20	max	0	0	0	0	0	2.6	0	2.6	0	2.6	0.084	2.6
187   5   M21   max   0.303   0   0.728   0   0   2.6   0   2.6   0   0.084   0     188   5   M22   max   1.482   0   0.16   0   0   0.284   0   0.284   0   0.284   1.724   0.094     190   min   1.417   6.284   0.004   6.284   0   0   0   0   0   0   0   0   0     191   5   M23   max   1.408   0   0.019   0   0   0   0   0   0   0   0   0				min	-0.027	2.6	-0.065	2.6	0	0	0	0	0	0	0	
188		5	M21			SERVED LOSSESSES.		200 K 2 B 2 C 2 C 2 C 2 C 2 C 2 C 2 C 2 C 2 C	0	26	0		AND DESCRIPTION OF THE PARTY OF	CONTRACTOR OF THE PARTY OF THE	0.084	ALTER MANAGEMENT PARTY
189   5   M22						1000000										
190		5	Maa			TROUGH (SET A COME		TOTAL CONTROL SECTION	A STATE OF THE PARTY OF THE PAR	The second second second	THE RESERVE THE PARTY OF THE PA					A DOLLAR OF THE PARTY OF THE PA
191   5		U	IVIZZ			10000000000000000000000000000000000000			CONTRACTOR OF THE PARTY OF THE				ALTO AND ALTO MANAGEMENT AND ADDRESS OF THE PARTY OF THE			
192		_	1.00	el gualitateless	AND RESIDENCE OF STREET	introduction to the control	AUGUSTANIA AND AND AND AND AND AND AND AND AND AN	110000000000000000000000000000000000000	PROPERTY AND PROPERTY.		PAGES OF STATE OF STATE OF	THE RESERVE TO BE SHOWN	CONTRACTOR		THE RESIDENCE OF THE REAL PROPERTY OF THE PARTY OF THE PA	A PART OF THE PART
193   5		5	M23	max		-										
194	_	000000		min		9.75	CONTRACTOR CONTRACTOR CONTRACTOR	THE PERSON NAMED IN COLUMN	Control of the Contro							
195   5	193	5	M24	max	1.338	0	-0.187	0	0	10.563	0	10.563	0	10.563	2.5	10.563
196	194			min	1.228	10.563	-0.451	10.563	0	0	0	0	0	0	-0.869	0
196	195	5	M25	max	1.338	10.563	0.451	0	0	10.563	0	10.563	0	10.563	2.5	0
197   5   M26				min				10.563	0	0	0	0	0	0	-0.869	10.563
198	THE RESERVE OF THE PARTY OF THE	5	M26		The comment of the control of the co	9 75	THE RESIDENCE OF THE PARTY OF T	0	0	9 75	0	9 75	Ō			0
199   5   M27   max   1.482   6.284   -0.004   0   0   6.284   0   6.284   0   0   6.284   0   0   0   0   0   0   0   0   0			11120											1 100		
200         min         1.417         0         -0.16         6.284         0         0         0         0         0         -2.24         0           201         5         M28         max         0.303         2.6         -0.663         0         0         2.6         0         2.6         0         2.6         0         2.6         0         2.6         0         0         0         0         -1.724         0           203         5         M29         max         0         2.6         0.065         0         0         2.6         0         2.6         0         2.6         0.084         0           204         min         -0.027         0         0         2.6         0		5	1/127			-		CONTRACTOR CONTRACTOR	U.S. Inches and Associated Property of the Control			_				PROPERTY AND ADDRESS OF THE PARTY OF THE PAR
201         5         M28         max         0.303         2.6         -0.663         0         0         2.6         0         2.6         0         0.084         2.6           202         min         0.276         0         -0.728         2.6         0         0         0         0         0         -1.724         0           203         5         M29         max         0         2.6         0.065         0         0         2.6         0         2.6         0         0.084         0           204         min         -0.027         0         0         2.6         0		O.	IVIZI													
202         min         0.276         0         -0.728         2.6         0         0         0         0         0         -1.724         0           203         5         M29         max         0         2.6         0.065         0         0         2.6         0         2.6         0         0         2.6         0	100000000000000000000000000000000000000	_	1400	THE RESERVE AND ADDRESS OF THE PERSON NAMED IN	\$1000 \$100 BIS 100 BIS		TAXABLE DESCRIPTION OF THE PROPERTY OF THE PRO	CONTRACTOR OF THE PERSON OF TH	CONTRACTOR OF THE PARTY OF THE					-		NAME OF TAXABLE PARTY.
203         5         M29         max         0         2.6         0.065         0         0         2.6         0         2.6         0		5	IVI28								-					
204         min -0.027         0         0         2.6         0		10204		min	0.276			Committee of the last of the l	AND DESCRIPTION OF THE PARTY OF		PART NO DESCRIPTION OF THE PARTY.					
205         5         M3         max -1.307         9.75         -0.056         9.75         0         9.75         0         9.75         0         9.75         0         9.75         0         9.75         0         9.75         0         9.75         0         9.75         0	203	5	M29	max		2.6	0.065	0	0	2.6	0	2.6	0	2.6	0.084	0
206         min -1.307         0         -0.056         0         0         0         0         0         0         0         -0.222         0           207         5         M4         max -1.307         9.75         0.056         9.75         0         9.75         0         9.75         0.329         0           208         min -1.307         0         0.056         0         0         0         0         0         0         0         -0.222         9.75           209         5         M5         max -1.307         9         -0.025         9         0         0         0	204			min	-0.027	0		2.6	0	0	0	0	0	0	0	2.6
206         min -1.307         0         -0.056         0         0         0         0         0         0         0         -0.222         0           207         5         M4         max -1.307         9.75         0.056         9.75         0         9.75         0         9.75         0.329         0           208         min -1.307         0         0.056         0         0         0         0         0         0         0         -0.222         9.75           209         5         M5         max -1.307         9         -0.025         9         0         0         0	205	5	M3	max	-1.307	9.75	-0.056	9.75	0	9.75	0	9.75	0	9.75	0.329	9.75
207         5         M4         max -1.307         9.75         0.056         9.75         0         9.75         0         9.75         0         9.75         0         9.75         0.329         0           208         min -1.307         0         0.056         0         0         0         0         0         0         0         -0.222         9.75           209         5         M5         max -1.307         9         -0.025         9         0         0         0         0         0         0									0		0		0			
208         min -1.307         0         0.056         0         0         0         0         0         0         0         -0.222         9.75           209         5         M5         max -1.307         9         -0.025         9         0         0         9         0		5	M4						THE RESERVE THE PROPERTY OF THE PARTY OF THE							
209 5         M5         max -1.307         9         -0.025         9         0         0		-	1111							1,000						
210         min -1.307         0         -0.025         0         0         0         0         0         0         -0.222         0           211         6         M1         max 3.004         5.8         0         5.8         0         5.8         0         5.8         0         5.8           212         min 3.004         0		5	MA					The state of the s	THE RESERVE AND ADDRESS OF THE PARTY.		THE SAME WAS ARREST OF THE PARTY OF THE PART					CONTROL OF THE PARTY OF THE PAR
211 6         M1         max 3.004         5.8         0         5.8         0         5.8         0         5.8         0         5.8         0         5.8         0         5.8         0         5.8         0 <td< td=""><td></td><td>U</td><td>UIU</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>		U	UIU													
212         min         3.004         0	210	_				THE OWNER OF THE OWNER OWNER OF THE OWNER OW	The state of the s		The state of the s							
213     6     M6     max     3.004     5.8     0     5.8     0     5.8     0     5.8     0     5.8     0     5.8       214     min     3.004     0     0     0     0     0     0     0     0     0     0     0     0       215     6     M7     max     0.061     2.417     0     2.417     0     2.417     0     2.417     0     2.417     0     2.417       216     min     0.061     0     0     0     0     0     0     0     0     0     0       217     6     M8     max     -0.185     6.167     0     6.167     0     6.167     0     6.167     0     6.167     0     6.167		6	M1				The state of the s									
214         min         3.004         0         2.417         0         2.417         0         2.417         0         2.417         0         2.417         0         2.417         0									ACTOR DESCRIPTION OF THE PROPERTY OF THE PROPE							
215         6         M7         max         0.061         2.417         0         2.417         0         2.417         0         2.417         0         2.417         0         2.417         0         2.417         0         2.417         0		6	M6			5.8	0	5.8	0	5.8	0	5.8	0	5.8	0	5.8
215         6         M7         max         0.061         2.417         0         2.417         0         2.417         0         2.417         0         2.417         0         2.417         0         2.417         0         2.417         0	214			min	3.004	0	0	0	0	0	0	0	0	0	0	0
216 min 0.061 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		6	M7			2.417	0	2.417	0	2.417	0	2.417			The second secon	
217 6 M8 max -0.185 6.167 0 6.167 0 6.167 0 6.167 0 6.167 0 6.167																
		6	M8				Andrew Street Book and the street									A RATE OF THE PARTY OF THE PART
		J	IVIO													
		G	N440				Martin and Springer Color			-						
		0	IVITU													6.167
220 min -0.185 0 0 0 0 0 0 0 0 0 0	[220]			Imin	J-U. 185	U	U	U	U	U	1 0	U	U	1 0	U	



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		illiulli Welliber S												
H-400H2000		Member Label			y Shear[k		z Shear[l	THE PERSON NAMED IN COLUMN	Tor que[k-	THE RESERVE TO A STREET OF THE PARTY OF THE	-y Moment[k-	COLUMN TAXABLE PROPERTY AND ADDRESS OF THE PARTY AND ADDRESS OF THE PAR	-z Moment[k-	
221	6	M11 ma	x 0.061	2.417	0	2.417	0	2.417	0	2.417	0	2.417	0	2.417
222		mi		0	0	0	0	0	0	0	0	0	0	0
223	6	M9 ma	x 0.257	10.23	0	10.23	0	10.23	0	10.23	0	10.23	0	10.23
224		mi		0	0	0	0	0	0	0	0	0	0	0
225	6	M2 ma	3.004	9	-0.057	9	0	9	0	9	0	9	0.509	9
226		mi	n 3.004	0	-0.057	0	0	0	0	0	0	0	0	0
227	6	M20 ma	x 0.062	2.6	0.149	2.6	0	2.6	0	2.6	0	2.6	0	0
228		mi	n 0	0	0	0	0	0	0	0	0	0	-0.194	2.6
229	6	M21 ma	-0.635	2.6	-1.523	2.6	0	2.6	0	2.6	0	2.6	3.96	2.6
230			n -0.697		-1.672	0	0	0	0	0	0	0	-0.194	0
231	6	M22 ma	x -3.26	6.284	-0.008	6.284	0	6.284	0	6.284	0	6.284	5.143	6.284
232		mi		0	-0.368	0	0	0	0	0	0	0	3.96	0
233	6		x -3.003		0.602	9.75	0	9.75	0	9.75	0	9.75	5.143	0
234		mi			0.043	0	0	0	0	0	0	0	1.996	9.75
235	6		x -2.822	A STATE OF THE PARTY OF THE PAR		10.563	0	10.563	0	10.563	0	10.563	1.996	0
236	0		n -3.074		0.43	0	0	0	0	0	0	0	-5.741	10.563
237	6		x -2.822		-0.43	10.563	0	10.563	0	10.563	0	10.563	1.996	10.563
238	U	mi		10.563		0	0	0	0	0	0		-5.741	
PLACE FOR THE LET	6		FORM THE PURE NOVEMBER OF THE PERSON NAMED IN	The second of the second	TABLE A STATE OF THE STATE OF T	of the supplemental to	PORTUGE STREET, STREET		Marie Control of the		The U.S. In section of the Control o	0 75		0 75
239	O		x -3.003		-0.043	9.75	0	9.75	0	9.75	0	9.75	5.143	9.75
240	0	MO7		100000000000000000000000000000000000000	-0.602	0	0	0	0	0	0	0	1.996	0
241	6	M27 ma		0	0.368	6.284	0	6.284	0	6.284	0	6.284	5.143	0
242	•	mi		6.284	0.008	0	0	0	0	0	0	0	3.96	6.284
243	6	M28 ma	AND DESCRIPTION OF THE PARTY OF		1.672	2.6	0	2.6	0	2.6	0	2.6	3.96	0
244		mi		THE RESERVE THE PARTY OF THE PA	1.523	0	0	0	0	0	0	0	-0.194	2.6
245	6	M29 ma	x 0.062	0	0	2.6	0	2.6	0	2.6	0	2.6	0	2.6
246		mi		2.6	-0.149	0	0	0	0	0	0	0	-0.194	0
247	6	M3 ma	x 3.004	9.75	0.13	9.75	0	9.75	0	9.75	0	9.75	0.509	0
248		mi	n 3.004	0	0.13	0	0	0	0	0	0	0	-0.756	9.75
249	6	M4 ma	3.004	9.75	-0.13	9.75	0	9.75	0	9.75	0	9.75	0.509	9.75
250		mi	n 3.004	0	-0.13	0	0	0	0	0	0	0	-0.756	0
251	6	M5 ma	x 3.004	9	0.057	9	0	9	0	9	0	9	0.509	0
252		mi	n 3.004	0	0.057	0	0	0	0	0	0	0	0	9
253	7	M1 ma	x-18.775	5.8	0	5.8	0	5.8	0	5.8	. 0	5.8	0	5.8
254			n -18.775		0	0	0	0	0	0	0	0	0	0
255	7	M6 ma	x-18.775	5.8	0	5.8	0	5.8	0	5.8	0	5.8	0	5.8
256			n -18.775		0	0	0	0	0	0	0	0	0	0
257	7	M7 ma	CALL FOR THE PARTY OF THE PARTY	-	0	2.417	0	2.417	0	2.417	0	2.417	0	2.417
258		mi		0	0	0	0	0	0	0	0	0	0	0
259	7	M8 ma			0	6.167	0	6.167	0	6.167	0	6.167	0	6.167
260	ELECTRICAL STATE OF	mi	Total	0.107	0	0.107	0	0.107	0	0.107	0	0.107	0	0.107
261	7	M10 ma		6.167	0	6.167	0	6.167	0	6.167	0	6.167	0	6.167
262	-			_	0		0			_				
263			n 1.237 x -0.177			2.417	0	2.417	0	2.417	0	2.417	0	2.417
264			n -0.177		0	0								
							0	0	0	0	0	0	0	0
265			x -1.743			10.23	0	10.23	0	10.23	0	10.23	0	10.23
266	-		n -1.743		0	0	0	0	0	0	0	0	0	0
267			1x-18.773		0.353	9	0	9	0	9	0	9	0	0
268			n -18.773	O CAROLINA CANADA CANADA	0.353	0	0	0	0	0	0	0	-3.181	9
269			x 0	0	-0.003	0	0	2.6	0	2.6	0	2.6	1.215	2.6
270			n -0.387		-0.932	2.6	0	0	0	0	0	0	0	0
271			x 4.346		10.49	0	0	2.6	0	2.6	0	2.6	1.215	0
272			n 3.959		9.561	2.6	0	0	0	0	0	0	-24.848	2.6
273			x21.217		2.312	0	0	6.284	0	6.284	0	6.284	-24.848	0
274			n 20.282			6.284	0	0	0	0	0	0	-32.325	6.284
275	7	M23 ma	x 20.212	0	-0.289	0	0	9.75	0	9.75	0	9.75	-12.525	9.75



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### Maximum Member Section Forces (Continued)

	LC	Member Labe	el	Axial[k]	Loc[ft]	y Shear[k]	Loc[ft]	z Shear[k	Loc[ft]	Tor que[k-f	ft]Loc[ft]	y-y Moment[k-ft	]Loc[ft]z	z-z Moment[k-	ft]Loc[ft]
276			min	18.761	9.75	-3.772	9.75	0	0	0	0	0	0	-32.325	0
277	7	M24	max	19.24	0	-2.71	0	0	10.563	0	10.563	0	10.563	36.022	10.563
278			min			-6.483	10.563	0	0	0	0	0	0	-12.525	0
279	7	M25	max	19.24	10.563	6.483	0	0	10.563	0	10.563	0	10.563	36.022	0
280			min	17.668	0	2.71	10.563	0	0	0	0	0	0	-12.525	10.563
281	7	M26	max	20.212	9.75	3.772	0	0	9.75	0	9.75	0	9.75	-12.525	0
282			min	18.761	0	0.289	9.75	0	0	0	0	0	0	-32.325	9.75
283	7	M27	max	21.217	6.284	-0.068	0	0	6.284	0	6.284	0	6.284	-24.848	6.284
284			min	20.282	0	-2.312	6.284	0	0	0	0	0	0	-32.325	0
285	7	M28	max	4.346	2.6	-9.561	0	0	2.6	0	2.6	0	2.6	1.215	2.6
286			min	3.959	0	-10.49	2.6	0	0	0	0	0	0	-24.848	0
287	7	M29	max	0	2.6	0.932	0	0	2.6	0	2.6	0	2.6	1.215	0
288			min	-0.387	0	0.003	2.6	0	0	0	0	0	0	0	2.6
289	7	M3	max	-18.777	9.75	-0.811	9.75	0	9.75	0	9.75	0	9.75	4.726	9.75
290			min	-18.777	0	-0.811	0	0	0	0	0	0	0	-3.181	0
291	7	M4	max	-18.777	9.75	0.811	9.75	0	9.75	0	9.75	0	9.75	4.726	0
292			min	-18.777	0	0.811	0	0	0	0	0	0	0	-3.181	9.75
293	7	M5	max	-18.773	9	-0.353	9	0	9	0	9	0	9	0	9
294			min	-18.773	0	-0.353	0	0	0	0	0	0	0	-3.181	0

#### Member Section Stresses

•		Member Label			v Shear[ksi]	z Shear[ksi]	v top Bendinalksil	y bot Bending[ksi] z	top Bendina[ksi]	z bot Bendina[ksi]
1	1	M1	1	-2.657	0	0	0	0	0	0
2			2	-2.657	0	0	0	0	0	0
3			3	-2.657	0	0	0	0	0	0
4			4	-2.657	0	0	0	0	0	0
5			5	-2.657	0	0	0	0	0	0
6	1	M6	1	-2.657	0	0	0	0	0	0
7			2	-2.657	0	0	0	0	0	0
8			3	-2.657	0	0	0	0	0	0
9			4	-2.657	0	0	0	0	0	0
10			5	-2.657	0	0	0	0	0	0
11	1	M7	1	-0.13	0	0	0	0	0	Ō
12			2	-0.13	0	0	0	0	0	0
13			3	-0.13	0	0	0	0	0	0
14			4	-0.13	0	0	0	0	0	0
15			5	-0.13	0	0	0	0	0	0
16	1	M8	1	0.528	0	0	0	0	0	0
17			2	0.528	0	0	0	0	0	0
18			3	0.528	0	0	0	0	0	0
19			4	0.528	0	0	0	0	0	0
20			5	0.528	0	0	0	0	0	0
21	1	M10	1	0.528	0	0	0	0	0	0
22			2	0.528	0	0	0	0	0	0
23	4		3	0.528	0	0	0	0	0	0
24			4	0.528	0	0	0	0	0	0
25			5	0.528	0	0	0	0	0	0
26	1	M11	1	-0.13	0	0	0	0	0	0
27			2	-0.13	0	0	0	0	0	0
28			3	-0.13	0	0	0	0	0	0
29			4	-0.13	0	0	0	0	0	0
30			5	-0.13	0	0	0	0	0	0
31	1	M9	1	-0.738	0	0	0	0	0	0
32			2	-0.738	0	0	0	0	0	0
33			3	-0.738	0	0	0	0	0	0



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34 35							7 1 31	7, 31, 3	z top zomamiginenj	z bot Bending[ksi]
	(30,000)		4	-0.738	0	0	0	0	0	0
			5	-0.738	0	0	0	0	0	0
	1	M2	1	-0.108	0.003	0	0	0	0	0
37			2	-0.108	0.003	0	0.036	-0.036	0	0
38			3	-0.108	0.003	0	0.073	-0.073	0	0
39			4	-0.108	0.003	0	0.109	-0.109	0	0
40		1400	5	-0.108	0.003	0	0.146	-0.146	0	0
STATISTICS STATE	1	M20	1	0	0	0	0	0	0	0
42	100000		2	0	-0.001	0	-0.001	0.001	0	0
43			3	-0.001	-0.002	0	-0.003	0.003	0	0
44		Note the second second second	4	-0.001	-0.003	0	-0.008	0.008	0	0
45		1404	5	-0.001	-0.004	0	-0.014	0.014	0	0
	1	M21	1	0.012	0.045	0	-0.014	0.014	0	0
47			2	0.012	0.044	0	0.063	-0.063	0	0
48	MASS D		3	0.012	0.043	0	0.139	-0.139	0	0
49			4	0.012	0.042	0	0.212	-0.212	0	0
50	4	1400	5	0.011	0.041	0	0.284	-0.284	0	0
DOMESTIC STREET	1	M22	1	0.061	0.01	0	0.284	-0.284	0	0
52	RESIDE D		2	0.06	0.008	0	0.321	-0.321	0	0
53			3	0.06	0.005	0	0.347	-0.347	0	0
54			4	0.059	0.003	0	0.363	-0.363	0	0
55	4	NACO	5	0.058	0	0	0.369	-0.369	0	0
	1	M23	1	0.058	-0.001	0	0.369	-0.369	0	0
57	N. W.		2	0.057	-0.005	0	0.349	-0.349	0	0
58	RESOL A		3	0.056	-0.009	0	0.305	-0.305	0	0
59			4	0.055	-0.012	0	0.236	-0.236	0	0
60	4	N40.4	5	0.054	-0.016	0	0.143	-0.143	0	0
	1	M24	1	0.055	-0.012	0	0.143	-0.143	0	0
62	50000		2	0.054	-0.016	0	0.047	-0.047	0	0
63			3	0.053	-0.02	0	-0.077	0.077	0	0
64 65			4	0.052	-0.024	0	-0.23	0.23	0	0
	4	NAOE	5	0.051	-0.028	0	-0.412	0.412	0	0
66 1 <b>67</b>	1	M25	1	0.051	0.028	0	-0.412 -0.23	0.412 0.23	0	0
68			2	0.052	0.024	0			0	
69			3	0.053 0.054	0.02	0	-0.077	0.077	0	0
70			5	0.054	0.016	0	0.047 0.143	-0.047 -0.143	0	0
December 2012 1900 270	1	M26	1	0.055	0.012 0.016	0	0.143	-0.143	0	0
72	1000	IVIZO	2	0.055	0.010	0	0.143	-0.143	0	0
73			3	0.056	0.009	0	0.305	-0.305	0	0
74	200		4	0.057	0.009	0	0.349	-0.349	0	0
75			5	0.058		0	0.369	-0.369		0
140000000	1	M27	1	0.058	0.001	0	0.369	-0.369	0	0
77	1	IVIZ /	2	0.056	-0.003	0	0.363	-0.363	0	0
78			3	0.039	-0.005	0	0.347	-0.347	0	0
79			4	0.06	-0.005	0	0.321	-0.347	0	0
80			5	0.061	-0.008	0	0.284	-0.284	0	0
CONTRACTOR STATE	1	M28	1	0.001	-0.01	0	0.284	-0.284	0	0
82	1 22	IVIZO	2	0.011	-0.041	0	0.212	-0.212	0	0
83			3	0.012	-0.042	0	0.139	-0.212	0	0
84	SHE CO.		4	0.012	-0.043	0	0.063	-0.139	0	0
85			5	0.012	-0.044	0	-0.014	0.014	0	0
	1	M29	1	-0.001	0.004	0	-0.014	0.014	0	0
87	-	IVICO	2	-0.001	0.004	0	-0.008	0.008	0	0
1 1 1 1	19835		3	-0.001	0.003	0	-0.003	0.003	0	0



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	LC	Member Labe						] y bot Bending[ksi]	The state of the second	
89			4	0	0.001	0	-0.001	0.001	0	0
90	100,00		5	0	0	0	0	0	0	0
91	1	M3	1	-0.108	-0.007	0	0.146	-0.146	0	0
92	No occupa		2	-0.108	-0.007	0	0.055	-0.055	0	0
93			3	-0.108	-0.007	0	-0.035	0.035	0	0
94	DOM:		4	-0.108	-0.007	0	-0.126	0.126	0	0
95		244	5	-0.108	-0.007	0	-0.217	0.217	0	0
96	1	M4	1	-0.108	0.007	0	-0.217	0.217	0	0
97			2	-0.108	0.007	0	-0.126	0.126	0	0
98			3	-0.108	0.007	0	-0.035	0.035	0	0
99			4	-0.108	0.007	0	0.055	-0.055	0	0
100	400	145	5	-0.108	0.007	0	0.146	-0.146	0	0
101	1	M5	1	-0.108	-0.003	0	0.146	-0.146	0	0
102	19000		2	-0.108	-0.003	0	0.109	-0.109	0	0
103			3	-0.108	-0.003	0	0.073	-0.073	0	0
104	Marini.		4	-0.108	-0.003	0	0.036	-0.036	0	0
105	_		5	-0.108	-0.003	0	0	0	0	0
106	2	M1	1	-7.097	0	0	0	0	0	0
107	6		2	-7.097	0	0	0	0	0	0
108	SUMMEN.		3	-7.097	0	0	0	0	0	0
109			4	-7.097	0	0	0	0	0	0
110			5	-7.097	0	0	0	0	0	0
111	2	M6	1	-7.097	0	0	0	0	0	0
112			2	-7.097	0	0	0	0	0	0
113			3	-7.097	0	0	0	0	0	0
114	BIRGINA		4	-7.097	0	0	0	0	0	0
115			5	-7.097	0	0	0	0	0	0
116	2	M7	1	-0.224	0	0	0	0	0	0
117			2	-0.224	0	0	0	0	0	0
118	NO CONTRACTOR		3	-0.224	0	0	0	0	0	0
119			4	-0.224	0	0	0	0	0	0
120			5	-0.224	0	0	0	0	0	0
121	2	M8	1	1.459	0	0	0	0	0	0
122		2 10 10 10 10 10 10 10 10 10 10 10 10 10	2	1.459	0	0	0	0	0	0
123			3	1.459	0	0	0	0	0	0
124			4	1.459	0	0	0	0	0	0
125			5	1.459	0	0	0	0	0	0
126	2	M10	1	1.459	0	0	0	0	0	0
127			2	1.459	0	0	0	0	0	0
128			3	1.459	0	0	0	0	0	0
129			4	1.459	0	0	0	0	0	0
130			5	1.459	0	0	0	0	0	0
131	2	M11	1	-0.224	0	0	0	0	0	0
132	N. S. Park		2	-0.224	0	0	0	0	0	0
133			3	-0.224	0	0	0	0	0	0
134			4	-0.224	0	0	0	0	0	0
135			5	-0.224	0	0	0	0	0	0
136	2	M9	1	-2.054	0	0	0	0	0	0
137			2	-2.054	0	0	0	0	0	0
138	in the second		3	-2.054	0	0	0	0	0	0
139			4	-2.054	0	0	0	0	0	0
140			5	-2.054	0	0	0	0	0	0
141	2	M2	1	-0.287	0.008	0	0	0	0	0
142			2	-0.287	0.008	0	0.097	-0.097	0	0
143			3	-0.287	0.008	0	0.195	-0.195	0	0



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144	LC	Member Lab		Axiai[ksi]	y Shear[ksi]		y top Bending[ks	i] y bot Bending[ksi]		
145	Magazia.		4	-0.287	0.008	0	0.292	-0.292	0	0
	2	MACO	5	-0.287	0.008	0	0.39	-0.39	0	0
146 147	2	M20	1	-0.001	-0.003	0	0	0	0	0
148			3	-0.001	-0.003	0	-0.002	0.002	0	0
149			4	-0.001	-0.005	0	-0.009	0.009	0	0
150			5			0	-0.021	0.021	0	0
151	2	M21	1	-0.003 0.033	-0.011 0.12	0	-0.037	0.037	0	0
152	2	IVIZ I	2	0.033		0	-0.037	0.037	0	0
153			3	0.033	0.118 0.115	0	0.169	-0.169	0	0
154	250500		4	0.032	0.113		0.371	-0.371	0	0
155			5	0.03	0.112	0	0.568 0.761	-0.568	0	0
156	2	M22	1	0.162	0.11	The second secon		-0.761	0	0
157		IVIZZ	2	0.162	0.027	0	0.761	-0.761	0	0
158			3	0.159		0	0.858	-0.858	0	0
159			4	0.159	0.014 0.007	0	0.929	-0.929	0	0
160			5	0.157	0.007	0	0.973	-0.973	0	0
161	2	M23	1	0.155	-0.003		0.989	-0.989	0	0
162	_	IVIZO	2	0.155	-0.003	0	0.989 0.935	-0.989 -0.935	, 0	0
163			3	0.132	-0.013	0	0.935		0	0
164			4	0.149	-0.023	0	0.632	-0.816	0	0
165			5	0.146	-0.033	0	0.383	-0.632	0	0
166	2	M24	1	0.144	-0.043	0	0.383	-0.383 -0.383	0	0
167		IVIZ4	2	0.147	-0.031	0	0.363	-0.383	0	0
168	4000000		3	0.144	-0.042	0			0	0
169			4	0.141	-0.064	0	-0.207 -0.617	0.207	0	0
170			5	0.135	-0.074	0	-0.617	0.617	0	0
171	2	M25	1	0.135	0.074	0	-1.103	1.103 1.103	0	0
172	2	IVIZO	2	0.138	0.074	0			0	0
173			3	0.138	0.053	0	-0.617 -0.207	0.617 0.207	0	0
174			4	0.141	0.033	0	0.126		0	0
175			5	0.147	0.042	0	0.383	-0.126 -0.383	0	0
176	2	M26	1	0.147	0.043	0	0.383	-0.383	0	0
177		IVIZO	2	0.144	0.043	0	0.632	-0.632	0	0
178	and the second		3	0.149	0.033	0	0.816	-0.816		
179			4	0.152	0.023	0	0.935	-0.935	0	0
180			5	0.155	0.003	0	0.989	-0.989	0	0
181	2	M27	1	0.155	-0.001	0	0.989	-0.989	0	0
182	_	IVIZI	2	0.157	-0.007	0	0.973	-0.969	0	0
183			3	0.157	-0.014	0	0.929	-0.929	0	0
184			4	0.161	-0.02	0	0.858	-0.858	0	0
185			5	0.162	-0.027	0	0.761	-0.761		
186	2	M28	1	0.102	-0.027	0	0.761	-0.761	0	0
187	_	IVIZU	2	0.031	-0.112	0	0.568	-0.568	0	0
188			3	0.031	-0.112	0	0.371	-0.371		
189			4	0.032	-0.118	0	0.169	-0.169	0	0
190			5	0.033	-0.118	0	-0.037	0.037		
	2	M29	1	-0.003	0.011	0	-0.037	0.037	0	0
192	-	IVIZU	2	-0.003	0.008	0	-0.037	0.037		0
193			3	-0.002	0.005	0	-0.009	0.009	0	0
194	reserve or a		4	-0.001	0.003	0	-0.009			
195			5	0	0.003	0	-0.002	0.002	0	0
196	2	M3	1	-0.287	-0.019	0	0.39	-0.39	0	
197	_	IVIO	2	-0.287	-0.019	0	0.39	-0.39	0	0
198	gets (134)		3	-0.287	-0.019	0	-0.095	0.095	0	0



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100	LC	Member Labe						i] y bot Bending[ksi]	Indicate and proceedings and process and p	TO THE OWNER OF THE PARTY OF TH
199			4	-0.287	-0.019	0	-0.337	0.337	0	0
200	0		5	-0.287	-0.019	0	-0.579	0.579	0	0
201	2	M4	1	-0.287	0.019	0	-0.579	0.579	0	0
202	165 3000		2	-0.287	0.019	0	-0.337	0.337	0	0
203			3	-0.287	0.019	0	-0.095	0.095	0	0
204			4	-0.287	0.019	0	0.147	-0.147	0	0
205	0	NA.	5	-0.287	0.019	0	0.39	-0.39	0	0
206	2	M5	1	-0.287	-0.008	0	0.39	-0.39	0	0
207			2	-0.287	-0.008	0	0.292	-0.292	0	0
208	No.		3	-0.287	-0.008	0	0.195	-0.195	0	0
209			4	-0.287	-0.008	0	0.097	-0.097	0	0
210	2	NAA	5	-0.287	-0.008	0	0	0	0	0
211	3	M1	1	0.159	0	0	0	0	0	0
212	No.		2	0.159	0	0	0	0	0	0
213			3	0.159	0	0	0	0	0	0
214			4	0.159	0	0	0	0	0	0
215	2	NAC	5	0.159	0	0	0	0	0	0
216	3	M6	1	0.159	0	0	0	0	0	0
217			2	0.159	0	0	0	0	0	0
218		The second second second	3	0.159	0	0	0	0	0	0
219 220			4	0.159	0	0	0	0	0	0
221	3	M7	5	0.159	0	0	0	0	0	0
	3	IVI /	1	0.009	0	0	0	0	0	0
222 223			3	0.009	0	0	0	0	0	0
224					0	0	0	0	0	0
225			4	0.009	0	0	0	0	0	0
	3	NAO	5		0	0	0	0	0	0
226 <b>227</b>	3	M8	1	-0.031	0	0	0	0	0	0
228			2	-0.031 -0.031	0	0	0	0	0	0
229			3	-0.031	0	0	0	0	0	0
230	120		5	-0.031	The second secon		0	0		0
231	3	M10	1	-0.031	0	0	0	0	0	0
232	3	IVITU	2	-0.031	0	0	. 0	0		0
233			3	-0.031	0	0	0		0	
234			4	-0.031	0	0	0	0	0	0
235			5	-0.031	0	0	0	0	0	0
236	3	M11	1	0.009	0	0	0	0	0	0
237	3	IVI I I	2	0.009	0	0	0	0	0	0
238			3	0.009	0	0	0			
239			4	0.009	0	0	0	0	0	0
240			5	0.009	0	0	0			
240 241	2	M9	1	0.009	0	0	0	0	0	0
242	J	IVI	2	0.043	0	0	0	0	0	0
242			3	0.043	0	0	0	0	0	0
243			4	0.043	0	0	0	0	0	0
245			5	0.043	0	0	0			
246	3	M2	1	0.043	0	0	0	0	0	0
247	J	IVIZ	2	0.006	0	0	-0.002	0.002	0	0
248			3	0.006			-0.002			
240 249			4	0.006	0	0	-0.004	0.004 0.007	0	0
250			5	0.006	0	0	-0.007			0
251	3	M20	1	THE REPORT OF THE PROPERTY OF THE PARTY OF	0	0		0.009	0	
251 252	J	IVIZU	2	0	0	0	0	0		0
252	(EZETERIO)		3	0	0	0	0	0	0	0



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	LC	Member Labe	Sec	Axial[ksi]	y Shear[ksi	z Shear[ksi]	y top Bending[ksi]	y bot Bending[ksi]	z top Bending[ksi]	z bot Bending[ksi]
254			4	0	0	0	0	0	0	0
255			5	0	0	0	0.001	-0.001	0	0
256	3	M21	1	-0.001	-0.003	0	0.001	-0.001	0	0
257			2	-0.001	-0.003	0	-0.004	0.004	0	0
258			3	-0.001	-0.003	0	-0.008	0.008	0	0
259			4	-0.001	-0.003	0	-0.013	0.013	0	0
260			5	-0.001	-0.002	0	-0.017	0.017	0	0
261	3	M22	1	-0.004	-0.001	0	-0.017	0.017	0	0
262			2	-0.004	0	0	-0.019	0.019	0	0
263			3	-0.004	0	0	-0.021	0.021	0	Ō
264			4	-0.004	0	0	-0.022	0.022	0	0
265			5	-0.003	Ö	0	-0.022	0.022	0	0
266	3	M23	1	-0.003	0	0	-0.022	0.022	0	0
267		WIZO	2	-0.003	Ö	0	-0.021	0.021	0	0
268			3	-0.003	0.001	0	-0.018	0.018	0	0
269			4	-0.003	0.001	0	-0.014	0.018	0	0
270		NAME   DECEMBER   DECEMBER   DECEMBER	5	-0.003	0.001	0	-0.009	0.009	0	0
271	3	M24	1	-0.003	0.001	0	-0.009		0	0
272	3	10124	-	-0.003				0.009		The second secon
	SERVICE S		2		0.001	0	-0.003	0.003	0	0
273			3	-0.003	0.001	0	0.005	-0.005	0	0
274		50 N , 7 10 10 20 10 10 10 10 10 10 10 10 10 10 10 10 10	4	-0.003	0.001	0	0.014	-0.014	0	0
275	•		5	-0.003	0.002	0	0.025	-0.025	0	0
276	3	M25	1	-0.003	-0.002	0	0.025	-0.025	0	0
277			2	-0.003	-0.001	0	0.014	-0.014	0	0
278			3	-0.003	-0.001	0	0.005	-0.005	0	0
279			4	-0.003	-0.001	0	-0.003	0.003	0	0
280			5	-0.003	-0.001	0	-0.009	0.009	0	0
281	3	M26	1	-0.003	-0.001	0	-0.009	0.009	0	0
282			2	-0.003	-0.001	0	-0.014	0.014	0	0
283			3	-0.003	-0.001	0	-0.018	0.018	0	0
284			4	-0.003	0	0	-0.021	0.021	0	0
285			5	-0.003	0	0	-0.022	0.022	0	0
286	3	M27	1	-0.003	0	0	-0.022	0.022	0	0
287			2	-0.004	0	0	-0.022	0.022	0	0
288			3	-0.004	0	0	-0.021	0.021	0	0
289			4	-0.004	0	0	-0.019	0.019	0	0
290			5	-0.004	0.001	0	-0.017	0.017	0	0
291	3	M28	1	-0.001	0.002	0	-0.017	0.017	0	0
292		WIZO	2	-0.001	0.003	0	-0.013	0.013	0	0
293			3	-0.001	0.003	0	-0.008	0.008	0	0
294	102.63		4	-0.001	0.003	0	-0.004	0.008	0	0
295			5	-0.001	0.003	0	0.001	-0.001	0	0
296		M29	1	0	0.003	0			0	0
297	J	IVIZƏ	2	0	0	disconnection were the present of	0.001	-0.001		
				ALTERNATION OF THE PERSON OF T		0	0	0	0	0
298			3	0	0	0	0	0	0	0
299			4	0	0	0	0	0	0	0
300	_		5	0	0	0	0	0	0	0
301	3	M3	1	0.006	0	0	-0.009	0.009	0	0
302	Call College		2	0.006	0	0	-0.003	0.003	0	0
303			3	0.006	0	0	0.002	-0.002	0	0
304			4	0.006	0	0	0.008	-0.008	0	0
305			5	0.006	0	0	0.013	-0.013	0	0
306	3	M4	1	0.006	0	0	0.013	-0.013	0	0
307			2	0.006	0	0	0.008	-0.008	0	0
308			3	0.006	0	0	0.002	-0.002	0	0



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	LC	Member Labe	Sec	Axial[ksi]	y Shear[ksi]:	z Shear[ksi]		] y bot Bending[ksi	z top Bending[ksi]	z bot Bending[ksi]
309			4	0.006	0	0	-0.003	0.003	0	0
310			5	0.006	0	0	-0.009	0.009	0	0
311	3	M5	1	0.006	0	0	-0.009	0.009	0	0
312			2	0.006	0	0	-0.007	0.007	0	0
313			3	0.006	0	0	-0.004	0.004	0	0
314			4	0.006	0	0	-0.002	0.002	0	0
315			5	0.006	0	0	0	0	0	Ō
316	4	M1	1	-4.978	0	0	0	0	0	0
317			2	-4.978	0	0	0	0	0	Ŏ
318			3	-4.978	0	0	0	0	0	0
319			4	-4.978	0	0	0	0	0	0
320		New York Control of the Control of t	5	-4.978	0	0	0	0	0	0
321	4	M6	1	-4.978	0	0	0	0	0	0
322		IVIO	2	-4.978	0	0	0	0		MANUAL REPORT OF THE RESIDENCE OF THE PROPERTY OF THE PARTY OF THE PAR
323			3	-4.978	0				0	0
	11.100			-4.978		0	0	0	0	0
324			4		0	0	0	0	0	0
325			5	-4.978	0	0	0	0	0	0
326	4	M7	1	-0.199	0	0	0	0	0	0
327			2	-0.199	0	0	0	0	0	0
328			3	-0.199	0	0	0	0	0	0
329			4	-0.199	0	0	0	0	0	0
330		1	5	-0.199	0	0	0	0	0	0
331	4	M8	1	1.006	0	0	0	0	0	0
332			2	1.006	0	0	0	0	0	0
333			3	1.006	0	0	0	0	0	0
334			4	1.006	0	0	0	0	0	0
335			5	1.006	0	0	0	0	0	0
336	4	M10	1	1.006	0	0	0	0	0	0
337			2	1.006	0	Ö	0	0	0	0
338			3	1.006	0	0	0	0	0	0
339			4	1.006	0	0	0	0	0	0
340			5	1.006	0	0	0	0	0	0
341	4	M11	1	-0.199	0	0	0	0	0	0
342		IVIII	2	-0.199	0	0	0	0		0
343			3	-0.199	0	0	0		0	0
344			4	-0.199	0	0		0		
345			5	-0.199			0	0	0	0
	4	NAO			0	0	0	0	0	0
346	4	M9	1	-1.412	0	0	0	0	0	0
347			2	-1.412	0	0	0	0	0	0
348	50000		3	-1.412	0	0	0	0	0	0
349			4	-1.412	0	0	0	0	0	0
350			5	-1.412	0	0	0	0	0	0
351	4	M2	1	-0.202	0.006	0	0	0	0	0
352		No. Contraction and the contraction of the contract	2	-0.202	0.006	0	0.068	-0.068	0	0
353			3	-0.202	0.006	0	0.137	-0.137	0	0
354			4	-0.202	0.006	0	0.205	-0.205	0	0
355			5	-0.202	0.006	0	0.273	-0.273	0	0
356	4	M20	1	0	0	0	0	0	0	0
357			2	-0.001	-0.002	0	-0.002	0.002	0	0
358			3	-0.001	-0.004	0	-0.007	0.007	0	0
359			4	-0.002	-0.006	0	-0.015	0.015	0	0
360			5	-0.002	-0.008	0	-0.015	0.015	0	0
361	4	M21	1	0.023	0.084	0	-0.026	0.026	0	0
		IVIZI	2	0.023	0.083	0	0.119	-0.119	0	0
362			1 4 1	0.023	0.003	U	0.119	I -U.119	1 U I	U



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	LC	Member Label	Sec	Axial[ksi]	y Shear[ksi]	z Shear[ksi]	y top Bending[ksi]	y bot Bending[ksi]	z top Bending[ksi]	z bot Bending[ksi]
364			4	0.022	0.079	0	0.398	-0.398	0	0
365			5	0.021	0.077	0	0.533	-0.533	0	0
366	4	M22	1	0.114	0.019	0	0.533	-0.533	0	0
367			2	0.113	0.014	0	0.601	-0.601	0	0
368			3	0.112	0.01	0	0.651	-0.651	0	0
369			4	0.11	0.005	0	0.681	-0.681	0	Ō
370			5	0.109	0.001	0	0.693	-0.693	0	0
371	4	M23	1	0.109	-0.002	O	0.693	-0.693	0	0
372			2	0.107	-0.009	0	0.655	-0.655	0	0
373			3	0.105	-0.016	0	0.572	-0.572	0	0
374	**************************************	UPC-04-21 AD 250-4 CA 73-95 EVOLUSIO ESPEC	4	0.103	-0.023	0	0.443	-0.443	0	0
375			5	0.101	-0.03	0	0.269	-0.269	0	0
376	4	M24	1	0.103	-0.022	0	0.269	-0.269	0	0
377		1012-1	2	0.101	-0.029	0	0.089	-0.089	0	0
378	March 197		3	0.099	-0.023	0	-0.145	0.145	0	0
379			4	0.097	-0.045	0	-0.432	0.432	0	0
380			5	0.095	-0.052	0	-0.432	0.432	0	0
381	4	M25	1	0.095	0.052	0	-0.773		AN ADMINISTRATION OF THE PARTY	
382	-	IVIZO	-	0.093				0.773	0	0
383			3	0.097	0.045 0.037	0	-0.432	0.432	0	0
						The state of the s	-0.145	0.145	0	0
384			4	0.101	0.029	0	0.089	-0.089	0	0
385		1400	5	0.103	0.022	0	0.269	-0.269	0	0
386	4	M26	1	0.101	0.03	0	0.269	-0.269	0	0
387			2	0.103	0.023	0	0.443	-0.443	0	0
388	United States	Name of the last o	3	0.105	0.016	0	0.572	-0.572	0	0
389			4	0.107	0.009	0	0.655	-0.655	0	0
390	ran sa tion to		5	0.109	0.002	0	0.693	-0.693	0	0
391	4	M27	1	0.109	-0.001	0	0.693	-0.693	0	0
392			2	0.11	-0.005	0	0.681	-0.681	0	0
393			3	0.112	-0.01	0	0.651	-0.651	0	0
394	Note of		4	0.113	-0.014	0	0.601	-0.601	0	0
395			5	0.114	-0.019	0	0.533	-0.533	0	0
396	4	M28	1	0.021	-0.077	0	0.533	-0.533	0	0
397			2	0.022	-0.079	0	0.398	-0.398	0	0
398			3	0.022	-0.081	0	0.26	-0.26	0	0
399			4	0.023	-0.083	0	0.119	-0.119	0	0
400			5	0.023	-0.084	0	-0.026	0.026	0	0
401	4	M29	1	-0.002	0.008	0	-0.026	0.026	0	0
402	a and		2	-0.002	0.006	0	-0.015	0.015	0	0
403			3	-0.001	0.004	0	-0.007	0.007	0	0
404			4	-0.001	0.002	0	-0.002	0.002	0	0
405			5	0	0	0	0.002	0.002	0	0
406	4	M3	1	-0.202	-0.013	0	0.273	-0.273	0	0
407			2	-0.202	-0.013	0	0.103	-0.103	0	0
408			3	-0.202	-0.013	0	-0.066	0.066	0	0
409			4	-0.202	-0.013	0	-0.236	0.236	0	0
410			5	-0.202	-0.013	0	-0.406	0.406	0	0
411	4	M4	1	-0.202	0.013	0	-0.406	0.406	0	0
412		IVIT	2	-0.202	0.013	0				
413			3	-0.202		0	-0.236	0.236	0	0
					0.013		-0.066	0.066	0	0
414			4	-0.202	0.013	0	0.103	-0.103	0	0
415		NAC.	5	-0.202	0.013	0	0.273	-0.273	0	0
416	4	M5	1	-0.202	-0.006	0	0.273	-0.273	0	0
417			2	-0.202	-0.006	0	0.205	-0.205	0	0
418			3	-0.202	-0.006	0	0.137	-0.137	0	0



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Checked By: JKF

		Member Labe		•		1z Shear[ksi]	v top Bendinalks	sil v bot Bending[ks	si] z top Bending[ksi]	z bot Bendina[ksi]
419			4	-0.202	-0.006	0	0.068	-0.068	0	0
420	Annual Control		5	-0.202	-0.006	0	0.000	0.000	0	0
421	5	M1	1	-0.531	0	0	0	Ŏ	0	0
422			2	-0.531	0	0	0	0	0	0
423			3	-0.531	Ō	0	0	0	0	0
424			4	-0.531	0	0	0	0	0	0
425			5	-0.531	0	0	0	o o	Ō	0
426	5	M6	1	-0.531	0	0	0	0	0	0
427		Acres de la companya	2	-0.531	0	0	0	0	Ō	0
428			3	-0.531	0	0	0	0	0	0
429			4	-0.531	0	0	0	0	0	0
430			5	-0.531	0	0	0	0	0	0
431	5	M7	1	-0.03	0	0	0	0	Ō	0
432			2	-0.03	0	0	0	0	0	0
433			3	-0.03	0	0	0	0	0	0
434			4	-0.03	0	0	0	0	0	0
435			5	-0.03	0	0	0	0	0	0
436	5	M8	1	0.104	0	0	0	0	0	0
437			2	0.104	0	0	0	0	0	0
438			3	0.104	0	0	0	0	0	0
439			4	0.104	0	0	0	0	-0	0
440			5	0.104	0	0	0	0	0	0
441	5	M10	1	0.104	0	0	0	0	0	0
442			2	0.104	0	0	0	0	0	0
443			3	0.104	0	0	0	0	0	0
444			4	0.104	0	0	0	0	0	0
445			5	0.104	0	0	0	0	0	0
446	5	M11	1	-0.03	0	0	0	0	0	0
447			2	-0.03	0	0	0	0	0	0
448			3	-0.03	0	0	0	0	0	0
449			4	-0.03	0	0	0	0	0	0
450			5	-0.03	0	0	0	0	0	0
451	5	M9	1	-0.145	0	0	0	0	0	0
452			2	-0.145	0	0	0	0	0	0
453			3	-0.145	0	0	0	0	0	0
454			4	-0.145	0	0	0	0	0	0
455			5	-0.145	0	0	0	0	0	0
456	5	M2	1	-0.022	0.001	0	0	0	0	0
457			2	-0.022	0.001	0	0.007	-0.007	0	0
458	No. of the		3	-0.022	0.001	0	0.015	-0.015	0	0
459			4	-0.022	0.001	0	0.022	-0.022	0	0
460	100 Etc. 1		5	-0.022	0.001	0	0.029	-0.029	0	0
461	5	M20	1	0	0	0	0	0	0	0
462	and the same		2	0	0	0	0	0	0	0
463			3	0	0	0	-0.001	0.001	0	0
464	90000000		4	0	-0.001	0	-0.002	0.002	0	0
465		110	5	0	-0.001	0	-0.003	0.003	0	0
466	5	M21	1	0.002	0.009	0	-0.003	0.003	0	0
467			2	0.002	0.009	0	0.013	-0.013	0	0
468			3	0.002	0.009	0	0.028	-0.028	0	0
469			4	0.002	0.008	0	0.042	-0.042	0	0
470		1400	5	0.002	0.008	0	0.057	-0.057	0	0
471	5	M22	1	0.012	0.002	0	0.057	-0.057	0	0
472			2	0.012	0.001	0	0.064	-0.064	0	0
473			3	0.012	0.001	0	0.069	-0.069	0	0



Company : MC Square Designer : Will Witkop Job Number : 2022-0507

: MC Squared : Will Witkop

Model Name: GOODWIN CHURCH GYM

10/10/2022 4:30:37 PM

Checked By: JKF

	LC	Member Labe	Sec	Axial[ksi]	v Shear[ksi]	z Shear[ksi]	v top Bendina[ksi]	v bot Bendina[ksi]	z top Bending[ksi]	z bot Bendina[ksi]
474			4	0.012	0.001	0	0.073	-0.073	0	0
475			5	0.012	0	0	0.074	-0.074	0	Ö
476	5	M23	1	0.012	0	0	0.074	-0.074	0	0
477			2	0.011	-0.001	0	0.07	-0.07	0	0
478			3	0.011	-0.002	0	0.061	-0.061	0	0
479			4	0.011	-0.002	Ō	0.047	-0.047	0	0
480	Mark Control		5	0.011	-0.003	0	0.029	-0.029	0	0
481	5	M24	1	0.011	-0.002	0	0.029	-0.029	0	0
482			2	0.011	-0.003	0	0.009	-0.009	0	0
483			3	0.011	-0.004	Ō	-0.015	0.015	0	0
484			4	0.01	-0.005	0	-0.046	0.046	0	0
485			5	0.01	-0.006	0	-0.082	0.082	0	0
486	5	M25	1	0.01	0.006	0	-0.082	0.082	0	0
487			2	0.01	0.005	Ö	-0.046	0.046	0	0
488			3	0.011	0.004	0	-0.015	0.015	0	0
489			4	0.011	0.003	0	0.009	-0.009	0	0
490			5	0.011	0.002	0	0.029	-0.029	0	0
491	5	M26	1	0.011	0.003	Ō	0.029	-0.029	0	0
492			2	0.011	0.002	0	0.047	-0.047	0	0
493			3	0.011	0.002	0	0.061	-0.061	0	0
494			4	0.011	0.001	0	0.07	-0.07	0	0
495			5	0.012	0	0	0.074	-0.074	0	0
496	5	M27	1	0.012	0	0	0.074	-0.074	0	0
497			2	0.012	-0.001	0	0.073	-0.073	0	0
498			3	0.012	-0.001	0	0.069	-0.069	0	0
499			4	0.012	-0.001	0	0.064	-0.064	0	0
500			5	0.012	-0.002	0	0.057	-0.057	0	0
501	5	M28	1	0.002	-0.008	0	0.057	-0.057	0	0
502			2	0.002	-0.008	0	0.042	-0.042	0	0
503			3	0.002	-0.009	0	0.028	-0.028	0	0
504			4	0.002	-0.009	0	0.013	-0.013	0	0
505			5	0.002	-0.009	0	-0.003	0.003	0	0
506	5	M29	1	0	0.001	0	-0.003	0.003	0	0
507			2	0	0.001	0	-0.002	0.002	0	0
508			3	0	0	0	-0.001	0.001	0	0
509			4	0	0	0	0	0	0	0
510			5	0	0	0	0	0	0	0
511	5	M3	1	-0.022	-0.001	0	0.029	-0.029	0	0
512			2	-0.022	-0.001	0	0.011	-0.011	0	0
513			3	-0.022	-0.001	0	-0.007	0.007	0	0
514			4	-0.022	-0.001	0	-0.025	0.025	0	0
515			5	-0.022	-0.001	0	-0.043	0.043	0	0
516	5	M4	1	-0.022	0.001	0	-0.043	0.043	0	0
517			2	-0.022	0.001	0	-0.025	0.025	0	0
518			3	-0.022	0.001	0	-0.007	0.007	0	0
519			4	-0.022	0.001	0	0.011	-0.011	0	0
520			5	-0.022	0.001	0	0.029	-0.029	0	0
521	5	M5	1	-0.022	-0.001	0	0.029	-0.029	0	0
522			2	-0.022	-0.001	0	0.022	-0.022	0	0
523			3	-0.022	-0.001	0	0.015	-0.015	0	0
524			4	-0.022	-0.001	0	0.007	-0.007	0	0
525			5	-0.022	-0.001	0	0	0	0	0
526	6	M1	1	1.221	0	0	0	0	0	0
527			2	1.221	0	0	0	0	0	0
528			3	1.221	0	0	0	0	0	0



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Checked By: JKF

	STATE OF	Member Label	Da			z Shear[ksi]	v top Bendina[ksi	] y bot Bending[ksi]	z top Bendina[ksi]	z bot Bendina[ksi]
529		THE THE COLUMN	4	1.221	0	0	0		0	0
530	10000000		5	1.221	0	0	0	0	0	0
531	6	M6	1	1.221	0	0	0	0	0	0
532		1110	2	1.221	0	0	0	0	0	0
533			3	1.221	Ö	0	0	0	0	0
534			4	1.221	0	0	0	0	0	0
535			5	1.221	Ö	0	0	0	0	0
536	6	M7	1	0.078	0	0	0	0	0	0
537			2	0.078	0	0	0	0	0	0
538			3	0.078	0	0	0	0	0	0
539			4	0.078	0	0	Ō	Ö	0	Ō
540			5	0.078	0	0	0	0	0	0
541	6	M8	1	-0.235	0	0	0	0	0	0
542			2	-0.235	0	0	0	0	0	0
543			3	-0.235	0	0	0	0	0	0
544			4	-0.235	0	0	0	0	0	0
545			5	-0.235	0	0	0	0	0	0
546	6	M10	1	-0.235	0	0	0	0	0	0
547			2	-0.235	0	0	0	0	0	0
548			3	-0.235	0	0	0	0	0	0
549			4	-0.235	0	0	0	0	0	0
550			5	-0.235	0	0	0	0	0	0
551	6	M11	1	0.078	0	0	0	0	0	0
552			2	0.078	0	0	0	0	0	0
553			3	0.078	0	0	0	0	0	0
554			4	0.078	0	0	0	0	0	0
555			5	0.078	0	0	0	0	0	0
556	6	M9	1	0.327	0	0	0	0	0	0
557			2	0.327	0	0	0	0	0	0
558			3	0.327	0	0	0	0	0	0
559			4	0.327	0	0	0	0	0	0
560			5	0.327	0	0	0	0	0	0
561	6	M2	1	0.049	-0.001	0	0	0	0	0
562			2	0.049	-0.001	0	-0.017	0.017	0	0
563			3	0.049	-0.001	0	-0.034	0.034	0	0
564			4	0.049	-0.001	0	-0.05	0.05	0	0
565			5	0.049	-0.001	0	-0.067	0.067	0	0
566	6	M20	1	0	0	0	0	0	0	0
567			2	0	0	0	0	0	0	0
568			3	0	0.001	0	0.002	-0.002	0	0
569			4	0	0.001	0	0.004	-0.004	0	0
570			5	0.001	0.002	0	0.006	-0.006	0	0
571	6	M21	1	-0.006	-0.021	0	0.006	-0.006	0	0
572			2	-0.006	-0.02	0	-0.029	0.029	0	0
573			3	-0.005	-0.02	0	-0.064	0.064	0	0
574	ENGLISHE -		4	-0.005	-0.019	0	-0.097	0.097	0	0
575			5	-0.005	-0.019	0	-0.13	0.13	0	0
576	6	M22	1	-0.028	-0.005	0	-0.13	0.13	0	0
577			2	-0.028	-0.003	0	-0.147	0.147	0	0
578			3	-0.027	-0.002	0	-0.159	0.159	0	0
579			4	-0.027	-0.001	0	-0.167	0.167	0	0
580			5	-0.027	0	0	-0.169	0.169	0	0
581	6	M23	1	-0.027	0.001	0	-0.169	0.169	0	0
582			2	-0.026	0.002	0	-0.16	0.16	0	0
583			3	-0.026	0.004	0	-0.14	0.14	0	0



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1000									z bot Bending[ksi]
ugme,		4	-0.025	0.006	0	-0.108	0.108	0	0
		5	-0.025	0.007	0	-0.066	0.066	0	0
6	M24	1	-0.025	0.005	0	-0.066	0.066	0	0
		2	-0.025	0.007	0	-0.022	0.022	0	0
		3	-0.024	0.009	0				0
		4	-0.024	0.011	0			0	0
		5	-0.023	0.013	0	0.189		0	0
6	M25	1	-0.023	-0.013	0	0.189	-0.189	0	0
		2	-0.024	-0.011	0	0.106	-0.106	0	0
		3	-0.024	-0.009	0	0.035	-0.035	0	0
		4	-0.025	-0.007	0	-0.022	0.022	0	0
		5		-0.005	0	-0.066	0.066	0	0
6	M26	1	-0.025	-0.007	0	-0.066	0.066	0	0
		2	-0.025	-0.006	0	-0.108	0.108	0	0
		3	-0.026	-0.004	0	-0.14	0.14	0	0
		4			0	-0.16	0.16	0	0
		5		-0.001	0	-0.169	0.169	0	0
6	M27	1	-0.027	0	0	-0.169	0.169	0	0
		2	-0.027	0.001	0	-0.167	0.167	0	0
		3		0.002	0	-0.159	0.159	0	0
		4		0.003	0	-0.147	0.147	0	0
		5		0.005	0		0.13	0	0
6	M28	1		0.019	0		0.13	0	0
					0	-0.097		0	0
		and the second second	Control of the Contro		0	-0.064	0.064	0	0
					0	-0.029	0.029	0	0
		100000000000000000000000000000000000000			0			0	0
6	M29	on this take					-0.006	0	0
			RASSESSED SERVICES		AND DESCRIPTION OF THE PERSON		-0.004	0	0
		3		-0.001	0	0.002	-0.002	0	0
SHOW SECTION			The second secon				0	0	0
			THE RESIDENCE AND ADDRESS.	Control of the Contro	THE RESERVE THE PARTY OF THE PA			0	0
6	M3	_						0	0
					The second secon				0
390001									0
		_							0
		100000000000000000000000000000000000000							0
6	M4	AND DESCRIPTION OF THE PERSON							0
20000000			The state of the s						0
		_							0
100200									0
_									0
6	M5				ACCUPATION OF CHARGOS STREET,				0
		_							0
		T 100 / 100							0
					***************************************				0
7	.,,,								0
1	IVI1								0
100,000									0
									0
		_				Contract Con			0
7	NAC								0
/	IVID							THE RESERVE THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NAMED IN COLU	0
SEE									0
	6	6 M29 6 M29 6 M3 6 M4 6 M5	3         4         5         6       M25         1         2         3         4         5         6       M26         1         2         3         4         5         6       M27         1         2         3         4         5         6       M28         1         2         3         4         5         6       M29         1         2         3         4         5         6       M3         1         2         3         4         5         6       M4         1         2         3         4         5         6       M4         1         2         3         4         5         6	3	3   -0.024   0.009     4   -0.024   0.011     5   -0.023   0.013   6   M25   1   -0.023   -0.013   2   -0.024   -0.001   3   -0.024   -0.009   4   -0.025   -0.007   5   -0.025   -0.007   5   -0.025   -0.007   6   M26   1   -0.025   -0.006   -0.002   -0.003   -0.002   -0.005   -0.002   -0.005   -0.002   -0.005   -0.002   -0.005   -0.002   -0.001   -0.002   -0.001   -0.002   -0.001   -0.002   -0.001   -0.002   -0.001   -0.002   -0.001   -0.002   -0.001   -0.002   -0.001   -0.003   -0.001   -0.003   -0.	3   -0.024   0.009   0	3 -0.024	3   -0.024   0.009   0   0.035   -0.035	3   -0.024   0.009   0   0.035   -0.035   0     4   -0.024   0.011   0   0.106   -0.106   0     5   -0.023   0.013   0   0.189   -0.189   0     2   -0.024   -0.011   0   0.189   -0.189   0     3   -0.024   -0.011   0   0.106   -0.106   0     4   -0.025   -0.007   0   0.035   -0.035   0     4   -0.025   -0.007   0   -0.022   0.022   0     5   -0.025   -0.007   0   -0.066   0.066   0     6   M26   1   -0.025   -0.007   0   -0.066   0.066   0     2   -0.025   -0.007   0   -0.066   0.066   0     3   -0.026   -0.006   0   -0.14   0.14   0     4   -0.026   -0.002   0   -0.16   0.16   0     5   -0.027   -0.001   0   -0.169   0.169   0     6   M27   1   -0.027   0   0   -0.169   0.169   0     6   M27   1   -0.027   0   0   -0.169   0.169   0     6   M27   1   -0.027   0   0   -0.169   0.169   0     6   M28   1   -0.028   0.003   0   -0.167   0     5   -0.028   0.003   0   -0.169   0.169   0     6   M28   1   -0.028   0.003   0   -0.147   0.147   0     6   M28   1   -0.028   0.003   0   -0.147   0.147   0     6   M28   1   -0.028   0.005   0   -0.13   0.13   0     6   M28   1   -0.005   0.019   0   -0.13   0.13   0     6   M28   1   -0.005   0.019   0   -0.037   0.097   0.097   0.097     6   M28   1   -0.005   0.019   0   -0.037   0.097   0.



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	LC	Member Label	Sec	Axial[ksi]	y Shear[ksi]	z Shear[ksi]	y top Bending[ksi]	y bot Bending[ksi]	z top Bending[ksi]	z bot Bending[ksi]
639			4	-7.63	0	0	0	0	0	0
640			5	-7.63	0	0	0	0	0	0
641	7	M7	1	-0.225	0	0	0	0	0	0
642			2	-0.225	0	0	0	0	0	0
643			3	-0.225	0	0	0	0	0	0
644			4	-0.225	0	0	0	0	0	0
645			5	-0.225	0	0	0	0	0	0
646	7	M8	1	1.575	0	0	0	0	0	0
647			2	1.575	0	0	0	0	0 - 1	0
648			3	1.575	0	0	0	0	0	0
649			4	1.575	0	0	0	0	0	0
650			5	1.575	0	0	0	0	0	0
651	7	M10	1	1.575	0	0	0	0	0	0
652			2	1.575	0	0	0	0	0	0
653			3	1.575	0	0	0	0	0	. 0
654			4	1.575	0	0	0	0	0	0
655			5	1.575	0	0	0	0	0	0
656	7	M11	1	-0.225	0	0	0	0	0	0
657			2	-0.225	0	0	0	0	0	0
658			3	-0.225	0	0	0	0	0	0
659			4	-0.225	0	0	0	0	0	0
660			5	-0.225	0	0	0	0	0	0
661	7	M9	1	-2.219	0	0	0	0	0	0
662			2	-2.219	0	0	0	0	0	0
663			3	-2.219	0	0	0	0	0	0
664			4	-2.219	0	0	0	0	0	0
665			5	-2.219	0	0	0	0	0	0
666	7	M2	1	-0.309	0.009	0	0	0	0	0
667			2	-0.309	0.009	0	0.105	-0.105	0	0
668			3	-0.309	0.009	0	0.209	-0.209	0	0
669			4	-0.309	0.009	0	0.314	-0.314	0	0
670			5	-0.309	0.009	0	0.419	-0.419	0	0
671	7	M20	1	0	0	0	0	0	0	0
672			2	-0.001	-0.003	0	-0.003	0.003	0	0
673			3	-0.002	-0.006	0	-0.01	0.01	0	0
674			4	-0.002	-0.009	0	-0.023	0.023	0	0
675			5	-0.003	-0.012	0	-0.04	0.04	0	0
676	7	M21	1	0.036	0.13	0	-0.04	0.04	0	0
677			2	0.035	0.127	0	0.182	-0.182	0	0
678			3	0.034	0.124	0	0.399	-0.399	0	0
679			4	0.033	0.121	0	0.611	-0.611	0	0
680			5	0.033	0.118	0	0.818	-0.818	0	0
681	7	M22	1	0.175	0.029	0	0.818	-0.818	0	0
682			2	0.173	0.022	0	0.923	-0.923	. 0	0
683			3	0.171	0.015	0	0.999	-0.999	0	0
684			4	0.169	0.008	0	1.046	-1.046	0	0
685			5	0.167	0.001	0	1.064	-1.064	0	0
686	7	M23	1	0.166	-0.004	0	1.064	-1.064	0	0
687			2	0.163	-0.014	0	1.006	-1.006	0	0
688			3	0.16	-0.025	0	0.878	-0.878	0	0
689			4	0.157	-0.036	0	0.68	-0.68	0	0
690			5	0.154	-0.047	0	0.412	-0.412	0	0
691		M24	1	0.158	-0.033	0	0.412	-0.412	0	0
692			2	0.155	-0.045	0	0.136	-0.136	0	0
693			3	0.152	-0.057	0	-0.223	0.223	0	0



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### Member Section Stresses (Continued)

	LC	Member Labe	el Sec	Axial[ksi]	y Shear[ksi]	z Shear[ksi	y top Bending[ks	i] y bot Bending[ksi] z	top Bending[ksi]	z bot Bending[ksi]
694			4	0.149	-0.068	0	-0.663	0.663	0	0
695			5	0.145	-0.08	0	-1.186	1.186	0	0
696	7	M25	1	0.145	0.08	0	-1.186	1.186	0	0
697			2	0.149	0.068	0	-0.663	0.663	0	0
698			3	0.152	0.057	0	-0.223	0.223	0	0
699			4	0.155	0.045	0	0.136	-0.136	0	0
700			5	0.158	0.033	0	0.412	-0.412	0	0
701	7	M26	1	0.154	0.047	0	0.412	-0.412	0	0
702			2	0.157	0.036	0	0.68	-0.68	0	0
703			3	0.16	0.025	0	0.878	-0.878	0	0
704			4	0.163	0.014	0	1.006	-1.006	0	0
705			5	0.166	0.004	0	1.064	-1.064	0	0
706	7	M27	1	0.167	-0.001	0	1.064	-1.064	0	0
707			2	0.169	-0.008	0	1.046	-1.046	0	0
708	STATE OF THE PARTY		3	0.171	-0.015	0	0.999	-0.999	0	0
709			4	0.173	-0.022	0	0.923	-0.923	0	0
710	ERRICH SON		5	0.175	-0.029	0	0.818	-0.818	0	0
711	7	M28	1	0.033	-0.118	0	0.818	-0.818	Ō	0
712	ALC: ALC:	WIZO	2	0.033	-0.121	0	0.611	-0.611	0	0
713			3	0.034	-0.124	0	0.399	-0.399	0	0
714	STATE OF THE PARTY.		4	0.035	-0.127	0	0.182	-0.182	0	0
715			5	0.036	-0.13	0	-0.04	0.04	0	0
716	7	M29	1	-0.003	0.012	0	-0.04	0.04	0	0
717		10123	2	-0.002	0.009	0	-0.023	0.023	0	0
718	averuse		3	-0.002	0.006	0	-0.01	0.01	0	0
719			4	-0.002	0.003	0	-0.003	0.003	0	0
720			5	0	0.000	0	0	0.000	0	0
721	7	M3	1	-0.309	-0.02	0	0.419	-0.419	0	0
722		IVIO	2	-0.309	-0.02	0	0.159	-0.159	0	0
723	10000		3	-0.309	-0.02	0	-0.102	0.102	0	0
724	200000	Committee and the state of the	4	-0.309	-0.02	0	-0.362	0.362	0	0
725			5	-0.309	-0.02	0	-0.622	0.622	0	0
726		M4	1	-0.309	0.02	0	-0.622	0.622	0	0
727		1014	2	-0.309	0.02	0	-0.362	0.362	0	0
728	B. 10.10.10		3	-0.309	0.02	0	-0.102	0.102	0	0
729	1239X 33		4	-0.309	0.02	0	0.159	-0.159	0	0
730			5	-0.309	0.02	0	0.139	-0.139	0	0
730		M5	1	-0.309	-0.009	0	0.419	-0.419	0	0
	1	CIVI	2	-0.309	-0.009	0	0.419	-0.314	0	0
732				-0.309	-0.009		0.209	-0.314	0	0
733			3			0		-0.209	0	0
734			4	-0.309	-0.009	0	0.105		0	0
735			5	-0.309	-0.009	0	0	0	U	U

#### Beam Deflection Checks

	Beam	Design Rule	Span	Defl [in]	Ratio	LC	Defl [in]	Ratio	LC	Defl [in]	Ratio	LC
1	M2	Typical	1	-0.013	8011	1(1)	-0.036	3001	2(1+2)	0	NC	3(1+4)
2	M20	Typical	1	1.388e-17	NC	1(1)	0	NC	2(1+2)	-8.674e-19	NC	3(1+4)
3	M21	Typical	1	0.0009799	NC	1(1)	0.0009456	NC	2(1+2)	-6.686e-5	NC	3(1+4)
4	M22	Typical	1	-0.015	4998	1(1)	-0.04	1867	2(1+2)	0	NC	3(1+4)
5	M23	Typical	1	-0.031	3715	1(1)	-0.084	1388	2(1+2)	0	NC	3(1+4)
6	M24	Typical	1	0.013	9684	1(1)	0.035	3615	2(1+2)	0	NC	3(1+4)
7	M25	Typical	1	0.013	9684	1(1)	0.035	3615	2(1+2)	0	NC	3(1+4)
8	M26	Typical	1	-0.031	3715	1(1)	-0.084	1388	2(1+2)	0	NC	3(1+4)
9	M27	Typical	1	-0.015	4998	1(1)	-0.04	1867	2(1+2)	1.735e-18	NC	3(1+4)
10	M28	Typical	1	1.388e-17	NC	1(1)	4.163e-17	NC	2(1+2)	0	NC	3(1+4)



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### Beam Deflection Checks (Continued)

	Beam	Design Rule	Span	Defl [in]	Ratio	LC	Defl [in]	Ratio	LC	Defl [in]	Ratio	LC
11	M29	Typical	1	-0.0002798	NC	1(1)	-0.0007493	NC	2(1+2)	1.674e-5	NC	3(1+4)
12	M3	Typical	1	0	NC	1(1)	0.028	4140	2(1+2)	0	NC	3(1+4)
13	M4	Typical	1	0	NC	1(1)	0.028	4140	2(1+2)	0	NC	3(1+4)
14	M5	Typical	1	-0.013	8011	1(1)	-0.036	3001	2(1+2)	0	NC	3(1+4)

#### AISC 15TH (360-16): ASD Member Steel Code Checks

	LC	Member	Shape	UC Max	Loc[ft]	Shear UC	Loc[ft]	Pnc/om [k]	Pnt/om [k]	Mnyy/om [k-f	t] Mnzz/om [k-ft]	Cb	Eqn
1	1	M1	HR2	0.123	5.8	0	5.8	14.948	53.042	1.565	1.565	1	H1-1b*
2	1	M6	HR2	0.123	5.8	0	5.8	14.948	53.042	1.565	1.565	1	H1-1b*
3	1	M7	GYMNASIUMBARS	0.006	2.417	0	2.417	8.336	16.931	0.282	0.282	1	H1-1b*
4	1	M8	GYMNASIUMBARS	0.308	6.167	0	6.167	1.347	16.931	0.282	0.282	1	H1-1a*
5	1	M10	<b>GYMNASIUMBARS</b>	0.308	6.167	0	6.167	1.347	16.931	0.282	0.282	1	H1-1a*
6	1	M11	GYMNASIUMBARS	0.006	2.417	0	2.417	8.336	16.931	0.282	0.282	1	H1-1b*
7	1	M9	<b>GYMNASIUMBARS</b>	0.034	10.23	0	10.23	0.49	16.931	0.282	0.282	1	H1-1b*
8	2	M1	HR2	0.329	5.8	0	5.8	14.948	53.042	1.565	1.565	1	H1-1a*
9	2	M6	HR2	0.329	5.8	0	5.8	14.948	53.042	1.565	1.565	1	H1-1a*
10	2	M7	GYMNASIUMBARS	0.01	2.417	0	2.417	8.336	16.931	0.282	0.282	1	H1-1b*
11	2	M8	GYMNASIUMBARS	0.85	6.167	0	6.167	1.347	16.931	0.282	0.282	1	H1-1a*
12	2	M10	GYMNASIUMBARS	0.85	6.167	0	6.167	1.347	16.931	0.282	0.282	1	H1-1a*
13	2	M11	GYMNASIUMBARS	0.01	2.417	0	2.417	8.336	16.931	0.282	0.282	1	H1-1b*
14	2	M9	GYMNASIUMBARS	0.095	10.23	0	10.23	0.49	16.931	0.282	0.282	1	H1-1b*
15	3	M1	HR2	0.026	5.8	0	5.8	14.948	53.042	1.565	1.565	1	H1-1b*
16	3	M6	HR2	0.026	5.8	0	5.8	14.948	53.042	1.565	1.565	1	H1-1b*
17	3	M7	GYMNASIUMBARS	0.001	2.417	0	2.417	8.336	16.931	0.282	0.282	1	H1-1b*
18	3	M8	GYMNASIUMBARS	0.001	6.167	0	6.167	1.347	16.931	0.282	0.282	1	H1-1b*
19	3	M10	GYMNASIUMBARS	0.001	6.167	0	6.167	1.347	16.931	0.282	0.282	1	H1-1b*
20	3	M11	GYMNASIUMBARS	0.001	2.417	0	2.417	8.336	16.931	0.282	0.282	1	H1-1b*
21	3	M9	GYMNASIUMBARS	0.069	10.23	0	10.23	0.49	16.931	0.282	0.282	1	H1-1b*
22	4	M1	HR2	0.231	5.8	0	5.8	14.948	53.042	1.565	1.565	1	H1-1a*
23	4	M6	HR2	0.231	5.8	0	5.8	14.948	53.042	1.565	1.565	1	H1-1a*
24	4	M7	GYMNASIUMBARS	0.009	2.417	0	2.417	8.336	16.931	0.282	0.282	1	H1-1b*
25	4	M8	GYMNASIUMBARS	0.587	6.167	0	6.167	1.347	16.931	0.282	0.282	1	H1-1a*
26	4	M10	GYMNASIUMBARS	0.587	6.167	0	6.167	1.347	16.931	0.282	0.282	1	H1-1a*
27	4	M11	<b>GYMNASIUMBARS</b>	0.009	2.417	0	2.417	8.336	16.931	0.282	0.282	1	H1-1b*
28	4	M9	GYMNASIUMBARS	0.066	10.23	0	10.23	0.49	16.931	0.282	0.282	1	H1-1b*
29	5	M1	HR2	0.025	5.8	0	5.8	14.948	53.042	1.565	1.565	1	H1-1b*
30	5	M6	HR2	0.025	5.8	0	5.8	14.948	53.042	1.565	1.565	1	H1-1b*
31	5	M7	<b>GYMNASIUMBARS</b>	0.001	2.417	0	2.417	8.336	16.931	0.282	0.282	1	H1-1b*
32	5	M8	GYMNASIUMBARS	0.06	6.167	0	6.167	1.347	16.931	0.282	0.282	1	H1-1b*
33	5	M10	<b>GYMNASIUMBARS</b>	0.06	6.167	0	6.167	1.347	16.931	0.282	0.282	1	H1-1b*
34	5	M11	GYMNASIUMBARS	0.001	2.417	0	2.417	8.336	16.931	0.282	0.282	1	H1-1b*
35	5	M9	<b>GYMNASIUMBARS</b>	0.007	10.23	0	10.23	0.49	16.931	0.282	0.282	1	H1-1b*
36	6	M1	HR2	0.201	5.8	0	5.8	14.948	53.042	1.565	1.565	1	H1-1a*
37	6	M6	HR2	0.201	5.8	0	5.8	14.948	53.042	1.565	1.565	1	H1-1a*
38	6	M7	GYMNASIUMBARS	0.007	2.417	0	2.417	8.336	16.931	0.282	0.282	1	H1-1b*
39	6	M8	<b>GYMNASIUMBARS</b>	0.011	6.167	0	6.167	1.347	16.931	0.282	0.282	1	H1-1b*
40	6	M10	GYMNASIUMBARS	0.011	6.167	0	6.167	1.347	16.931	0.282	0.282	1	H1-1b*
41	6	M11	<b>GYMNASIUMBARS</b>	0.007	2.417	0	2.417	8.336	16.931	0.282	0.282	1	H1-1b*
42	6	M9	GYMNASIUMBARS	0.524	10.23	0	10.23	0.49	16.931	0.282	0.282	1	H1-1a*
43	7	M1	HR2	0.354	5.8	0	5.8	14.948	53.042	1.565	1.565	1	H1-1a*
44	7	M6	HR2	0.354	5.8	0	5.8	14.948	53.042	1.565	1.565	1	H1-1a*
45	7	M7	<b>GYMNASIUMBARS</b>	0.01	2.417	0	2.417	8.336	16.931	0.282	0.282	1	H1-1b*
46	7	M8	GYMNASIUMBARS	0.918	6.167	0	6.167	1.347	16.931	0.282	0.282	1	H1-1a*
47	7	M10	<b>GYMNASIUMBARS</b>	0.918	6.167	0	6.167	1.347	16.931	0.282	0.282	1	H1-1a*
48	7	M11	GYMNASIUMBARS	0.01	2.417	0	2.417	8.336	16.931	0.282	0.282	1	H1-1b*



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#### AISC 15TH (360-16): ASD Member Steel Code Checks (Continued)

	LC	Member	Shape	<b>UC Max</b>	Loc[ft]	Shear UC	Loc[ft]	Pnc/om [k	Pnt/om [k]	Mnyy/om [k-ft]	] Mnzz/om [k-ft]	Cb	Eqn
49	7	M9	<b>GYMNASIUMBARS</b>	0.103	10.23	0	10.23	0.49	16.931	0.282	0.282	1	H1-1b*

#### AWC NDS-18: ASD Member Wood Code Checks

The color   The	Eqn
2   M20   6.75X18FS   0.007   2.6   0.013   2.6   v   1.592   1.1   2.396   1.45   0.3   3.5110.9990.995     4   1   M21   6.75X18FS   0.159   0.6   0.15   0   v   1.592   1.1   2.396   1.45   0.3   3.5110.9990.995     5   1   M23   6.75X18FS   0.156   6.284   0.033   0   v   1.591   1.1   2.395   1.45   0.3   5.4580.9960.963     6   1   M24   6.75X18FS   0.175   0   0.054   9.75   v   1.399   1.1   2.385   1.45   0.3   7.0760.9930.825     7   1   M25   6.75X18FS   0.175   0   0.093   0   v   1.327   1.1   2.384   1.45   0.3   7.0760.9930.825     8   1   M26   6.75X18FS   0.157   0.054   0   v   1.397   1.1   2.384   1.45   0.3   7.0760.9930.825     9   1   M27   6.75X18FS   0.157   0.054   0   v   1.399   1.1   2.385   1.45   0.3   7.0760.9930.825     9   1   M27   6.75X18FS   0.157   0.054   0   v   1.399   1.1   2.385   1.45   0.3   7.0760.9930.825     10   1   M28   6.75X18FS   0.156   0   0.033   6.284   v   1.594   1.1   2.395   1.45   0.3   3.5480.9960.963     10   1   M28   6.75X18FS   0.156   0   0.033   6.284   v   1.594   1.1   2.396   1.45   0.3   3.5110.9990.985     12   1   M3   6.75X18FS   0.119   0   0.15   2.6   v   1.592   1.1   2.396   1.45   0.3   3.5110.9990.985     12   1   M3   6.75X18FS   0.188   0   0.023   9.75   v   1.391   1.1   2.393   1.45   0.3   3.5110.9990.995     13   1   M4   6.75X9FS   0.188   0   0.023   9.75   v   1.391   1.1   2.393   1.45   0.3   4.8070.9970.865     14   1   M29   6.75X18FS   0.016   2.6   0.031   2.6   v   1.829   1.265   2.755   1.667   0.345   3.5110.9990.995     15   2   M21   6.75X18FS   0.016   2.6   0.031   2.6   v   1.829   1.265   2.755   1.667   0.345   3.5110.9990.995     18   2   M22   6.75X18FS   0.369   6.284   0.077   0   v   1.759   1.265   2.755   1.667   0.345   3.5110.9990.995     18   2   M22   6.75X18FS   0.369   6.284   0.077   0   v   1.759   1.265   2.755   1.667   0.345   3.5110.9990.995     19   M24   6.75X18FS   0.376   0   0.016   0   0.31   0   v   1.484   1.265   2.755   1.667   0.345   3.5110.9990.995     18   2   M24   6.	3.9-1
1	
4 1         M22 6,75X18FS 0.156         6.284 0.033         0 v         1.541         1.1         2.391         1.45         0.3         5.4880.9960.963           6 1         M24 6,75X18FS 0.175         10.00         0.054         9.75 y         1.397         1.1         2.384         1.45         0.3         6.7990.9940.868           7 1         M25 6,75X18FS 0.175 10.563         0.093         10.563 y         1.327         1.1         2.384         1.45         0.3         7.0760.9930.828           8 1         M26 6,75X18FS 0.175 0         0.093         0 y         1.327 1.1         2.384         1.45 0.3         7.0760.9930.828           9 1         M27 6,75X18FS 0.156         0         0.033         6.284 y         1.541 1.1         2.395 1.45         0.3         5.7990.9940.868           9 1         M27 6,75X18FS 0.156         0         0.033         6.284 y         1.541 1.1         2.396 1.45         0.3         5.54580.9960.963           10 1         M28 6,75X18FS 0.0159 0         0         0.013 0 y         1.592 1.1         2.396 1.45         0.3         3.5110.9990.998           12 1 1         M36 6,75X9FS 0.188 0         0         0.023 9.75 y         1.391 1.1         2.396 1.45         0.3         3.48070.9970.898	
6         1         M23         6.75X18FS         0.175         0         0.064         9.75         y         1.39         1.1         2.385         1.45         0.3         6.790,994,086           7         1         M25         6.75X18FS         0.175         0         0.093         0         y         1.327         1.1         2.384         1.45         0.3         7.076()993().828           8         1         M26         6.75X18FS         0.1175         0.064         0         y         1.39         1.1         2.384         1.45         0.3         6.790()994().868           9         1         M26         6.75X18FS         0.156         0         0.033         6.284         y         1.541         1.1         2.395         1.45         0.3         5.510()990()990()990()990()990()990()990()9	
6 1         M24 6,75X18FS 0.175 0.563 0.093 10.563 y 1.327 1.1 2.384 1.45 0.3 7.0760.9930.825           7 1         M25 6,75X18FS 0.175 0.00.093 0 y 1.327 1.1 2.384 1.45 0.3 7.0760.9930.825           8 1         M26 6,75X18FS 0.157 9.75 0.054 0 y 1.399 1.1 2.385 1.45 0.3 6.7990.9940.866           9 1         M27 6,75X18FS 0.156 0 0 0.033 6.284 y 1.541 1.1 2.391 1.45 0.3 5.4580.996.963           10 1         M28 6,75X18FS 0.119 0 0 0.15 2.6 y 1.592 1.1 2.396 1.45 0.3 3.5110.9990.995           11 1         M29 6,75X18FS 0.198 0 0.07 0 0.013 0 y 1.592 1.1 2.396 1.45 0.3 3.5110.9990.995           12 1         M3 6,75X9FS 0.188 0 0.07 0 0.013 0 y 1.592 1.1 2.396 1.45 0.3 4.8070.9970.895           13 1         M4 6,75X9FS 0.188 0 0.002 3 9.75 y 1.391 1.1 2.393 1.45 0.3 4.8070.9970.895           13 1         M4 6,75X9FS 0.188 0 0 0.023 9.75 y 1.391 1.1 2.393 1.45 0.3 4.8070.9970.895           14 1         M5 6,75X9FS 0.159 0 0.01 9 y 1.438 1.1 2.394 1.45 0.3 4.8070.9970.895           15 2         M2 6,75X9FS 0.159 0 0.01 9 y 1.438 1.1 2.394 1.45 0.3 4.6190.9970.895           16 2         M20 6,75X18FS 0.368 9 0.024 9 y 1.607 1.265 2.755 1.667 0.345 3.5110.9980.994           17 2         M21 6,75X18FS 0.369 6.284 0.077 0 y 1.829 1.265 2.755 1.667 0.345 3.5110.9980.994           18 2         M22 6,75X18FS 0.369 6.284 0.077 0 y 1.759 1.265 2.748 1.667 0.345 6.7990.9930.835           20 2         M24 6,75X18FS 0.3415 0 0.216 0 0.216 0.05 y 1.536 1.265 2.755 1.667 0.345 6.7990.9930.835	3.9-3
T	
8	
9   1   M27   6.75X18FS   0.156   0   0.033   6.284   y   1.541   1.1   2.391   1.45   0.3   5.4580.9960.963     10   1   M28   6.75X18FS   0.119   0   0.15   2.6   y   1.592   1.1   2.396   1.45   0.3   3.5110.9990.995     11   M29   6.75X18FS   0.179   0   0.013   0   y   1.592   1.1   2.396   1.45   0.3   3.5110.9990.995     12   1   M3   6.75X9FS   0.188   9.75   0.023   9.75   y   1.391   1.1   2.393   1.45   0.3   4.8070.9970.869     13   1   M4   6.75X9FS   0.188   0   0.023   9.75   y   1.391   1.1   2.393   1.45   0.3   4.8070.9970.869     14   1   M5   6.75X9FS   0.159   0   0.01   9   y   1.438   1.1   2.394   1.45   0.3   4.6190.9970.893     15   2   M2   6.75X18FS   0.168   9   0.024   9   y   1.607   1.265   2.752   1.667   0.345   4.6190.9970.893     16   2   M20   6.75X18FS   0.016   2.6   0.031   2.6   y   1.829   1.265   2.755   1.667   0.345   3.5110.9980.994     17   2   M21   6.75X18FS   0.276   2.6   0.349   0   y   1.829   1.265   2.755   1.667   0.345   3.5110.9980.994     18   2   M22   6.75X18FS   0.369   6.284   0.077   0   y   1.759   1.265   2.748   1.667   0.345   5.4580.996.996     19   2   M23   6.75X18FS   0.369   6.284   0.077   0   y   1.759   1.265   2.748   1.667   0.345   5.4580.996.996     2   M23   6.75X18FS   0.415   10.563   0.216   10.563   y   1.444   1.265   2.739   1.667   0.345   5.4580.996.996     2   M24   6.75X18FS   0.415   10.563   0.216   0.549   y   1.536   1.265   2.744   1.667   0.345   6.7990.9930.835     2   M25   6.75X18FS   0.369   0   0.077   6.284   y   1.759   1.265   2.755   1.667   0.345   6.7990.9930.835     2   M26   6.75X18FS   0.369   0   0.077   6.284   y   1.759   1.265   2.755   1.667   0.345   6.7990.9930.835     2   M27   6.75X18FS   0.369   0   0.077   6.284   y   1.759   1.265   2.755   1.667   0.345   6.7990.9930.835     2   M28   6.75X18FS   0.369   0   0.077   6.284   y   1.759   1.265   2.755   1.667   0.345   6.7990.9930.835     2   M28   6.75X18FS   0.369   0   0.014   0   0   0.126   0   0.014   0   0.014   0.014   0.014   0.01	
1	
11   1   M29   6.75X18FS   0.007   0   0.013   0   y   1.592   1.1   2.396   1.45   0.3   3.5110.9990.995   12   1   M3   6.75X9FS   0.188   9.75   0.023   9.75   y   1.391   1.1   2.393   1.45   0.3   4.8070.9970.868   14   1   M5   6.75X9FS   0.188   0   0.023   9.75   y   1.391   1.1   2.393   1.45   0.3   4.8070.9970.868   14   1   M5   6.75X9FS   0.159   0   0.01   9   y   1.438   1.1   2.394   1.45   0.3   4.8070.9970.868   15   2   M2   6.75X9FS   0.368   9   0.024   9   y   1.607   1.265   2.752   1.667   0.345   4.6190.9970.873   16   2   M20   6.75X18FS   0.016   2.6   0.031   2.6   y   1.829   1.265   2.755   1.667   0.345   3.5110.9980.994   18   2   M21   6.75X18FS   0.366   6.284   0.077   0   y   1.759   1.265   2.755   1.667   0.345   3.5110.9980.994   18   2   M22   6.75X18FS   0.366   6.284   0.077   0   y   1.759   1.265   2.748   1.667   0.345   6.4580.9960.956   19   2   M23   6.75X18FS   0.374   0   0.126   9.75   y   1.536   1.265   2.739   1.667   0.345   6.7590.9930.835   2.2   2   M26   6.75X18FS   0.3415   0.216   10.563   y   1.444   1.265   2.739   1.667   0.345   7.0760.9920.785   2.2   2   M26   6.75X18FS   0.369   0.216   0   y   1.444   1.265   2.739   1.667   0.345   7.0760.9920.785   2.2   2   M26   6.75X18FS   0.369   0   0.077   6.284   y   1.759   1.265   2.755   1.667   0.345   5.4580.9960.956   2.2   M28   6.75X18FS   0.369   0   0.077   6.284   y   1.759   1.265   2.755   1.667   0.345   5.4580.9960.956   2.2   M28   6.75X18FS   0.369   0   0.077   6.284   y   1.759   1.265   2.755   1.667   0.345   5.4580.9960.956   2.2   M28   6.75X18FS   0.369   0   0.077   6.284   y   1.759   1.265   2.755   1.667   0.345   5.4580.9960.956   0.345   0.	
12   1   M3	3.9-1
13   1   M4   6.75X9FS   0.188   0   0.023   9.75   y   1.391   1.1   2.393   1.45   0.3   4.8070.9970.868   14   1   M5   6.75X9FS   0.159   0   0.01   9   y   1.438   1.1   2.394   1.45   0.3   4.6190.9970.878   15   2   M2   6.75X9FS   0.368   9   0.024   9   y   1.607   1.265   2.755   1.667   0.345   4.6190.9970.873   16   2   M20   6.75X18FS   0.016   2.6   0.031   2.6   y   1.829   1.265   2.755   1.667   0.345   3.5110.9980.994   17   2   M21   6.75X18FS   0.369   6.284   0.077   0   y   1.759   1.265   2.755   1.667   0.345   3.5110.9980.994   18   2   M22   6.75X18FS   0.369   6.284   0.077   0   y   1.759   1.265   2.748   1.667   0.345   3.5110.9980.994   18   2   M22   6.75X18FS   0.374   0   0.126   9.75   y   1.536   1.265   2.744   1.667   0.345   5.4580.9960.956   2   M23   6.75X18FS   0.341   0   0.126   9.75   y   1.536   1.265   2.739   1.667   0.345   7.0760.9920.785   2   M24   6.75X18FS   0.3415   0   0.216   0   y   1.444   1.265   2.739   1.667   0.345   7.0760.9920.785   2   M25   6.75X18FS   0.3415   0   0.216   0   y   1.444   1.265   2.739   1.667   0.345   7.0760.9920.785   2   M26   6.75X18FS   0.374   9.75   0.126   0   y   1.444   1.265   2.739   1.667   0.345   7.0760.9920.785   2   M26   6.75X18FS   0.369   0   0.077   6.284   y   1.536   1.265   2.748   1.667   0.345   5.4580.9960.956   2   M29   6.75X18FS   0.369   0   0.077   6.284   y   1.759   1.265   2.755   1.667   0.345   3.5110.9980.994   2   2   M28   6.75X18FS   0.368   0   0.031   0   y   1.829   1.265   2.755   1.667   0.345   3.5110.9980.994   2   2   M29   6.75X18FS   0.368   0   0.031   0   y   1.829   1.265   2.755   1.667   0.345   3.5110.9980.994   3   3   M28   6.75X18FS   0.437   0.054   9.75   y   1.536   1.265   2.755   1.667   0.345   3.5110.9980.996   3   3   M28   6.75X18FS   0.043   0.054   9.75   y   1.536   1.265   2.755   1.667   0.345   3.5110.9980.996   3   3   M28   6.75X18FS   0.043   0.054   9.75   y   1.536   1.265   2.755   1.667   0.345   3.5110.9980.996   3   3   M28   6.75X18FS   0.008	3.9-1
14         1         M5         6.75X9FS         0.159         0         0.01         9         y         1.438         1.1         2.394         1.45         0.3         4.6190.9970.839           15         2         M20         6.75X18FS         0.308         9         0.024         9         y         1.607         1.265         2.755         1.667         0.345         3.5110.9980.994           17         2         M21         6.75X18FS         0.276         2.6         0.349         0         y         1.829         1.265         2.755         1.667         0.345         3.5110.9980.994           18         2         M22         6.75X18FS         0.369         6.284         0.077         0         y         1.759         1.265         2.748         1.667         0.345         3.5110.9980.994           19         2         M23         6.75X18FS         0.374         0         0.126         9.75         y         1.536         1.265         2.748         1.667         0.345         5.7990.9930.835           20         2         M24         6.75X18FS         0.415         0         0.216         0         y         1.444         1.265         2	3.9-1
15   2   M2   6.75X19FS   0.368   9   0.024   9   y   1.607   1.265   2.752   1.667   0.345   4.619   0.997   0.873   16   2   M20   6.75X18FS   0.016   2.6   0.031   2.6   y   1.829   1.265   2.755   1.667   0.345   3.511   0.998   0.994   17   2   M21   6.75X18FS   0.369   6.264   0.077   0   y   1.759   1.265   2.755   1.667   0.345   3.511   0.998   0.994   18   2   M22   6.75X18FS   0.369   6.284   0.077   0   y   1.759   1.265   2.748   1.667   0.345   3.511   0.998   0.994   18   2   M23   6.75X18FS   0.374   0   0.126   9.75   y   1.536   1.265   2.74   1.667   0.345   6.799   0.993   0.835   20   2   M24   6.75X18FS   0.415   0.563   0.216   10.563   y   1.444   1.265   2.739   1.667   0.345   7.076   0.992   0.785   21   2   M25   6.75X18FS   0.415   0   0.216   0   y   1.444   1.265   2.739   1.667   0.345   7.076   0.992   0.785   22   M26   6.75X18FS   0.374   9.75   0.126   0   y   1.4344   1.265   2.744   1.667   0.345   7.076   0.992   0.785   22   M26   6.75X18FS   0.369   0   0.077   6.284   y   1.759   1.265   2.748   1.667   0.345   5.458   0.996   0.956   24   2   M28   6.75X18FS   0.369   0   0.077   6.284   y   1.759   1.265   2.748   1.667   0.345   3.511   0.998   0.994   2.5   2   M29   6.75X18FS   0.437   9.75   0.054   9.75   y   1.536   1.265   2.755   1.667   0.345   3.511   0.998   0.994   2.5   M29   6.75X18FS   0.437   9.75   0.054   9.75   y   1.536   1.265   2.751   1.667   0.345   3.511   0.998   0.994   2.5   M29   6.75X18FS   0.437   9.75   0.054   9.75   y   1.536   1.265   2.751   1.667   0.345   3.511   0.998   0.994   2.5   M29   6.75X18FS   0.437   0   0.054   9.75   y   1.536   1.265   2.751   1.667   0.345   3.511   0.998   0.994   2.5   M29   6.75X18FS   0.437   0   0.054   9.75   y   1.536   1.265   2.751   1.667   0.345   4.619   0.997   8.35   2.5   M29   6.75X18FS   0.437   0   0.054   9.75   y   1.536   1.265   2.751   1.667   0.345   4.619   0.997   0.751   0.545   0.554   0.554   0.554   0.555   0.5555   0.5555   0.5555   0.5555   0.5555   0.5555   0.5555	
16   2   M20   6.75X18FS   0.016   2.6   0.031   2.6   y   1.829   1.265   2.755   1.667   0.345   3.511   0.998   0.994   12   12   M21   6.75X18FS   0.276   2.6   0.349   0   y   1.829   1.265   2.755   1.667   0.345   3.511   0.998   0.994   18   2   M22   6.75X18FS   0.369   6.284   0.077   0   y   1.759   1.265   2.748   1.667   0.345   6.759   0.996   0.964   0.965   0.986   0.98	3.9-1
17         2         M21         6.75X18FS         0.276         2.6         0.349         0         y         1.829         1.265         2.755         1.667         0.345         3.511 0.998 0.994           18         2         M22         6.75X18FS         0.374         0         0.126         9.75         y         1.536         1.265         2.748         1.667         0.345         5.4580 0.996 0.956           19         2         M23         6.75X18FS         0.347         0         0.126         9.75         y         1.536         1.265         2.744         1.667         0.345         7.076 0.992 0.785           20         2         M24         6.75X18FS         0.415         0         0.216         0         y         1.444         1.265         2.739         1.667         0.345         7.076 0.992 0.785           21         2         M26         6.75X18FS         0.415         0         0.216         0         y         1.444         1.265         2.739         1.667         0.345         7.076 0.992 0.785           22         2         M26         6.75X18FS         0.349         2.6         y         1.536         1.265         2.748	3.9-1
18         2         M22         6.75X18FS         0.369         6.284         0.077         0         y         1.759         1.265         2.748         1.667         0.345         5.458 0.996 0.956           19         2         M23         6.75X18FS         0.344         0         0.126         9.75         y         1.536         1.265         2.74         1.667         0.345         6.7990.9930.835           20         2         M24         6.75X18FS         0.415         10.563         0.216         0         y         1.444         1.265         2.739         1.667         0.345         7.076 0.9920.785           21         2         M26         6.75X18FS         0.374         9.75         0.126         0         y         1.536         1.265         2.739         1.667         0.345         7.076 0.9920.785           22         M26         6.75X18FS         0.374         9.75         0.126         0         y         1.536         1.265         2.74         1.667         0.345         5.7990.993.835           23         2         M27         6.75X18FS         0.369         0         0.077         6.284         y         1.759         1.265 <t< td=""><td></td></t<>	
19   2   M23   6.75X18FS   0.374   0   0.126   9.75   y   1.536   1.265   2.74   1.667   0.345   6.7990.993 0.835    20   2   M24   6.75X18FS   0.415   10.563   0.216   10.563   y   1.444   1.265   2.739   1.667   0.345   7.0760.992 0.785    21   2   M25   6.75X18FS   0.415   0   0.216   0   y   1.444   1.265   2.739   1.667   0.345   7.0760.992 0.785    22   2   M26   6.75X18FS   0.374   9.75   0.126   0   y   1.536   1.265   2.74   1.667   0.345   6.7990.993 0.835    23   2   M27   6.75X18FS   0.369   0   0.077   6.284   y   1.759   1.265   2.748   1.667   0.345   5.4580.996 0.956    24   2   M28   6.75X18FS   0.276   0   0.349   2.6   y   1.829   1.265   2.755   1.667   0.345   3.5110.998 0.994    25   2   M29   6.75X18FS   0.016   0   0.031   0   y   1.829   1.265   2.755   1.667   0.345   3.5110.998 0.994    26   2   M3   6.75X9FS   0.437   9.75   0.054   9.75   y   1.536   1.265   2.751   1.667   0.345   4.8070.997 0.835    27   2   M4   6.75X9FS   0.437   0   0.054   9.75   y   1.536   1.265   2.751   1.667   0.345   4.8070.997 0.835    28   2   M5   6.75X9FS   0.368   0   0.024   9   y   1.607   1.265   2.751   1.667   0.345   4.619 0.996 0.785    29   3   M2   6.75X18FS   0.003   9   0   9   y   2   1.76   3.823   2.32   0.48   4.619 0.996 0.785    30   3   M20   6.75X18FS   0.003   9   0   9   y   2.539   1.76   3.831   2.32   0.48   3.5110.998 0.992    31   3   M21   6.75X18FS   0.008   6.218   0.001   0   y   2.382   1.76   3.831   2.32   0.48   5.458 0.994 0.93    33   3   M23   6.75X18FS   0.008   0   0.002   9.75   y   1.841   1.76   3.8   2.32   0.48   6.799 0.990 0.716    34   3   M24   6.75X18FS   0.008   0   0.002   9.75   y   1.841   1.76   3.8   2.32   0.48   6.799 0.990 0.716    35   3   M25   6.75X18FS   0.008   0.006   0.002   9.75   y   1.841   1.76   3.8   2.32   0.48   6.799 0.990 0.716    36   3   M26   6.75X18FS   0.008   0.065   0.001   6.284   y   2.382   1.76   3.816   2.32   0.48   5.458 0.994 0.93 0.65 0.65 0.001   6.284   y   2.382   1.76   3.816   2.32   0.48   5.458 0.994	
20         2         M24         6.75X18FS         0.415         10.563         0.216         10.563         y         1.444         1.265         2.739         1.667         0.345         7.076 0.992 0.785           21         2         M25         6.75X18FS         0.415         0         0.216         0         y         1.444         1.265         2.739         1.667         0.345         7.076 0.992 0.785           22         M26         6.75X18FS         0.374         9.75         0.126         0         y         1.536         1.265         2.74         1.667         0.345         6.799 0.993 0.835           23         2         M27         6.75X18FS         0.369         0         0.077         6.284         y         1.759         1.265         2.748         1.667         0.345         5.458 0.996 0.956           24         2         M29         6.75X18FS         0.016         0         0.349         2.6         y         1.829         1.265         2.755         1.667         0.345         3.5110.998 0.994         2.6         2         M3         6.75X9FS         0.437         9.75         0.054         9.75         y         1.536         1.265         2.751 <td></td>	
21         2         M25         6.75X18FS         0.415         0         0.216         0         y         1.444         1.265         2.739         1.667         0.345         7.076         0.992         0.785           22         2         M26         6.75X18FS         0.374         9.75         0.126         0         y         1.536         1.265         2.74         1.667         0.345         6.799         0.993         0.835           23         2         M27         6.75X18FS         0.369         0         0.077         6.284         y         1.759         1.265         2.748         1.667         0.345         5.458         0.996         0.956           24         M28         6.75X18FS         0.276         0         0.349         2.6         y         1.829         1.265         2.755         1.667         0.345         3.511         0.998         0.994           25         M29         6.75X18FS         0.016         0         0.031         0         y         1.829         1.265         2.755         1.667         0.345         4.807         0.997         0.835           27         M4         6.75X9FS         0.437 <th< td=""><td></td></th<>	
22         M26         6.75X18FS         0.374         9.75         0.126         0         y         1.536         1.265         2.74         1.667         0.345         6.799 0.993 0.835           23         2         M27         6.75X18FS         0.369         0         0.077         6.284         y         1.759         1.265         2.748         1.667         0.345         5.458 0.996 0.956         24         2         M28         6.75X18FS         0.276         0         0.349         2.6         y         1.829         1.265         2.755         1.667         0.345         3.511 0.998 0.994         2.6         y         1.829         1.265         2.755         1.667         0.345         3.511 0.998 0.994         2.6         2         M3         6.75X18FS         0.016         0         0.031         0         y         1.829         1.265         2.755         1.667         0.345         4.807 0.997 0.835         2.752         1.667         0.345         4.807 0.997 0.835         2.752         1.667         0.345         4.807 0.997 0.835         2.752         1.667         0.345         4.619 0.997 0.835         2.853         2.752         1.667         0.345         4.619 0.997 0.835         2.752         1.6	
23         2         M27         6.75X18FS         0.369         0         0.077         6.284         y         1.759         1.265         2.748         1.667         0.345         5.458 0.996 0.956           24         2         M28         6.75X18FS         0.276         0         0.349         2.6         y         1.829         1.265         2.755         1.667         0.345         3.511 0.998 0.994           25         2         M29         6.75X18FS         0.016         0         0.031         0         y         1.829         1.265         2.755         1.667         0.345         3.511 0.998 0.994           26         2         M3         6.75X9FS         0.437         9.75         0.054         9.75         y         1.536         1.265         2.751         1.667         0.345         4.807 0.997 0.835           27         2         M4         6.75X9FS         0.437         0         0.054         9.75         y         1.536         1.265         2.751         1.667         0.345         4.807 0.997 0.835           28         2         M5         6.75X9FS         0.368         0         0.024         9         y         1.667         1.265<	
24         2         M28         6.75X18FS         0.276         0         0.349         2.6         y         1.829         1.265         2.755         1.667         0.345         3.5110.9980.994           25         2         M29         6.75X18FS         0.016         0         0.031         0         y         1.829         1.265         2.755         1.667         0.345         3.5110.9980.994           26         2         M3         6.75X9FS         0.437         9.75         0.054         9.75         y         1.536         1.265         2.751         1.667         0.345         4.8070.9970.835           27         2         M4         6.75X9FS         0.437         0         0.054         9.75         y         1.536         1.265         2.751         1.667         0.345         4.8070.9970.835           28         2         M5         6.75X9FS         0.368         0         0.024         9         y         1.607         1.265         2.752         1.667         0.345         4.6190.9970.873           29         3         M2         6.75X18FS         0.003         9         0         9         y         2.539         1.76         3.8	
25         2         M29         6.75X18FS         0.016         0         0.031         0         y         1.829         1.265         2.755         1.667         0.345         3.511         0.998         0.994           26         2         M3         6.75X9FS         0.437         9.75         0.054         9.75         y         1.536         1.265         2.751         1.667         0.345         4.807         0.997         0.835           27         2         M4         6.75X9FS         0.437         0         0.054         9.75         y         1.536         1.265         2.751         1.667         0.345         4.807         0.997         0.835           28         2         M5         6.75X9FS         0.368         0         0.024         9         y         1.607         1.265         2.752         1.667         0.345         4.619         0.997         0.873           29         3         M2         6.75X9FS         0.003         9         0         9         y         2         1.76         3.823         2.32         0.48         4.619         0.990         0.91         2.539         1.76         3.831         2.32 <t< td=""><td></td></t<>	
26       2       M3       6.75X9FS       0.437       9.75       0.054       9.75       y       1.536       1.265       2.751       1.667       0.345       4.807 0.997 0.835         27       2       M4       6.75X9FS       0.437       0       0.054       9.75       y       1.536       1.265       2.751       1.667       0.345       4.807 0.997 0.835         28       2       M5       6.75X9FS       0.368       0       0.024       9       y       1.607       1.265       2.752       1.667       0.345       4.619 0.997 0.873         29       3       M2       6.75X9FS       0.003       9       0       9       y       2       1.76       3.823       2.32       0.48       4.619 0.996 0.781         30       3       M20       6.75X18FS       0       2.6       0       2.6       y       2.539       1.76       3.831       2.32       0.48       3.511 0.998 0.992         31       3       M21       6.75X18FS       0.005       2.6       0.006       0       y       2.382       1.76       3.816       2.32       0.48       3.511 0.998 0.992         32       3       M22       6.75X	
27         2         M4         6.75X9FS         0.437         0         0.054         9.75         y         1.536         1.265         2.751         1.667         0.345         4.807 0.997 0.835           28         2         M5         6.75X9FS         0.368         0         0.024         9         y         1.667         1.265         2.752         1.667         0.345         4.619 0.997 0.873           29         3         M2         6.75X9FS         0.003         9         0         9         y         2         1.76         3.823         2.32         0.48         4.619 0.996 0.781           30         3         M20         6.75X18FS         0         2.6         0         2.6         y         2.539         1.76         3.831         2.32         0.48         3.511 0.998 0.992           31         3         M21         6.75X18FS         0.005         2.6         0.006         0         y         2.539         1.76         3.831         2.32         0.48         3.511 0.998 0.992           32         3         M22         6.75X18FS         0.008         6.218         0.001         0         y         2.382         1.76         3.816	
28         2         M5         6.75X9FS         0.368         0         0.024         9         y         1.607         1.265         2.752         1.667         0.345         4.619         0.997         0.873           29         3         M2         6.75X9FS         0.003         9         0         9         y         2         1.76         3.823         2.32         0.48         4.619         0.996         0.781           30         3         M20         6.75X18FS         0         2.6         0         2.6         y         2.539         1.76         3.831         2.32         0.48         3.511         0.998         0.992           31         3         M21         6.75X18FS         0.005         2.6         0.006         0         y         2.539         1.76         3.831         2.32         0.48         3.511         0.998         0.992           32         3         M22         6.75X18FS         0.008         6.218         0.001         0         y         2.382         1.76         3.816         2.32         0.48         5.458         0.994         0.93           34         3         M24         6.75X18FS	3.9-1
29         3         M2         6.75X9FS         0.003         9         0         9         y         2         1.76         3.823         2.32         0.48         4.619 0.996 0.781           30         3         M20         6.75X18FS         0         2.6         0         2.6         y         2.539         1.76         3.831         2.32         0.48         3.511 0.998 0.992           31         3         M21         6.75X18FS         0.005         2.6         0.006         0         y         2.539         1.76         3.831         2.32         0.48         3.511 0.998 0.992           32         3         M22         6.75X18FS         0.008         6.218         0.001         0         y         2.382         1.76         3.816         2.32         0.48         5.458 0.994 0.93           33         3         M23         6.75X18FS         0.008         0         0.002         9.75         y         1.841         1.76         3.8         2.32         0.48         6.799 0.99 0.719           34         3         M24         6.75X18FS         0.008         0         0.003         0         y         1.663         1.76         3.796	
30         3         M20         6.75X18FS         0         2.6         0         2.6         y         2.539         1.76         3.831         2.32         0.48         3.5110.9980.992           31         3         M21         6.75X18FS         0.005         2.6         0.006         0         y         2.539         1.76         3.831         2.32         0.48         3.5110.9980.992           32         3         M22         6.75X18FS         0.008         6.218         0.001         0         y         2.382         1.76         3.816         2.32         0.48         5.4580.994         0.93           33         3         M23         6.75X18FS         0.008         0         0.002         9.75         y         1.841         1.76         3.8         2.32         0.48         6.799 0.99 0.719           34         3         M24         6.75X18FS         0.008         10.563         0.003         10.563         y         1.663         1.76         3.796         2.32         0.48         7.0760.989 0.65           35         3         M25         6.75X18FS         0.008         0         0.003         0         y         1.663         1.76	3.6.3
32       3       M22       6.75X18FS       0.008       6.218       0.001       0       y       2.382       1.76       3.816       2.32       0.48       5.458 0.994 0.93         33       3       M23       6.75X18FS       0.008       0       0.002       9.75       y       1.841       1.76       3.8       2.32       0.48       6.799 0.99 0.719         34       3       M24       6.75X18FS       0.008       10.563       0.003       10.563       y       1.663       1.76       3.796       2.32       0.48       7.076 0.989 0.65         35       3       M25       6.75X18FS       0.008       0       0.003       0       y       1.663       1.76       3.796       2.32       0.48       7.076 0.989 0.65         36       3       M26       6.75X18FS       0.008       9.75       0.002       0       y       1.841       1.76       3.8       2.32       0.48       6.799 0.99 0.719         37       3       M27       6.75X18FS       0.008       0.065       0.001       6.284       y       2.382       1.76       3.816       2.32       0.48       5.458 0.994       0.93         38       3	3.9-3
32       3       M22       6.75X18FS       0.008       6.218       0.001       0       y       2.382       1.76       3.816       2.32       0.48       5.458 0.994 0.93         33       3       M23       6.75X18FS       0.008       0       0.002       9.75       y       1.841       1.76       3.8       2.32       0.48       6.799 0.99 0.719         34       3       M24       6.75X18FS       0.008       10.563       0.003       10.563       y       1.663       1.76       3.796       2.32       0.48       7.076 0.989 0.65         35       3       M25       6.75X18FS       0.008       0       0.003       0       y       1.663       1.76       3.796       2.32       0.48       7.076 0.989 0.65         36       3       M26       6.75X18FS       0.008       9.75       0.002       0       y       1.841       1.76       3.8       2.32       0.48       6.799 0.99 0.719         37       3       M27       6.75X18FS       0.008       0.065       0.001       6.284       y       2.382       1.76       3.816       2.32       0.48       5.458 0.994       0.93         38       3	3.9-1
33       3       M23       6.75X18FS       0.008       0       0.002       9.75       y       1.841       1.76       3.8       2.32       0.48       6.799       0.99       0.719         34       3       M24       6.75X18FS       0.008       10.563       0.003       10.563       y       1.663       1.76       3.796       2.32       0.48       7.076       0.989       0.65         35       3       M25       6.75X18FS       0.008       0       0.003       0       y       1.663       1.76       3.796       2.32       0.48       7.076       0.989       0.65         36       3       M26       6.75X18FS       0.008       9.75       0.002       0       y       1.841       1.76       3.8       2.32       0.48       6.799       0.99       0.719         37       3       M27       6.75X18FS       0.008       0.065       0.001       6.284       y       2.382       1.76       3.816       2.32       0.48       5.458       0.994       0.93         38       3       M28       6.75X18FS       0.005       0       0.006       2.6       y       2.539       1.76       3.831	3.9-1
35     3     M25     6.75X18FS     0.008     0     0.003     0     y     1.663     1.76     3.796     2.32     0.48     7.076 0.989 0.65       36     3     M26     6.75X18FS     0.008     9.75     0.002     0     y     1.841     1.76     3.8     2.32     0.48     6.799 0.99 0.719       37     3     M27     6.75X18FS     0.008     0.065     0.001     6.284     y     2.382     1.76     3.816     2.32     0.48     5.458 0.994     0.93       38     3     M28     6.75X18FS     0.005     0     0.006     2.6     y     2.539     1.76     3.831     2.32     0.48     3.511 0.998 0.992	3.9-1
36     3     M26     6.75X18FS     0.008     9.75     0.002     0     y     1.841     1.76     3.8     2.32     0.48     6.799     0.99     0.719       37     3     M27     6.75X18FS     0.008     0.065     0.001     6.284     y     2.382     1.76     3.816     2.32     0.48     5.458 0.994     0.93       38     3     M28     6.75X18FS     0.005     0     0.006     2.6     y     2.539     1.76     3.831     2.32     0.48     3.511 0.998 0.992	3.9-1
37     3     M27     6.75X18FS     0.008     0.065     0.001     6.284     y     2.382     1.76     3.816     2.32     0.48     5.458 0.994     0.93       38     3     M28     6.75X18FS     0.005     0     0.006     2.6     y     2.539     1.76     3.831     2.32     0.48     3.511 0.998 0.992	3.9-1
38 3 M28 6.75X18FS 0.005 0 0.006 2.6 y 2.539 1.76 3.831 2.32 0.48 3.5110.998 0.992	3.9-1
	3.9-1
39 3 M29 6.75X18FS 0 0 0 0 y 2.539 1.76 3.831 2.32 0.48 3.5110.9980.992	3.9-1
	3.9-3
40 3 M3 6.75X9FS 0.004 9.75 0.001 9.75 V 1.841 1.76 3.822 2.32 0.48 4.807 0.995 0.719	3.6.3
41 3 M4 6.75X9FS 0.004 9.75 0.001 9.75 y 1.841 1.76 3.822 2.32 0.48 4.807 0.995 0.718	3.6.3
42 3 M5 6.75X9FS 0.003 9 0 9 y 2 1.76 3.823 2.32 0.48 4.6190.9960.781	3.6.3
43 4 M2 6.75X9FS 0.186 9 0.012 9 y 2 1.76 3.823 2.32 0.48 4.619 0.996 0.781	
44 4 M20 6.75X18FS 0.008 2.6 0.016 2.6 y 2.539 1.76 3.831 2.32 0.48 3.5110.9980.992	3.9-1
45 4 M21 6.75X18FS 0.139 2.6 0.176 0 y 2.539 1.76 3.831 2.32 0.48 3.5110.9980.992	
46 4 M22 6.75X18FS 0.184 6.284 0.039 0 y 2.382 1.76 3.816 2.32 0.48 5.458 0.994 0.93	
47 4 M23 6.75X18FS 0.187 0 0.063 9.75 y 1.841 1.76 3.8 2.32 0.48 6.799 0.99 0.719	
48 4 M24 6.75X18FS 0.208 10.563 0.109 10.563 y 1.663 1.76 3.796 2.32 0.48 7.076 0.989 0.65	3.9-3
49 4 M25 6.75X18FS 0.208 0 0.109 0 y 1.663 1.76 3.796 2.32 0.48 7.076 0.989 0.65	3.9-3
50 4 M26 6.75X18FS 0.187 9.75 0.063 0 y 1.841 1.76 3.8 2.32 0.48 6.799 0.99 0.719	3.9-3
51 4 M27 6.75X18FS 0.184 0 0.039 6.284 y 2.382 1.76 3.816 2.32 0.48 5.4580.994 0.93	3.9-3



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Checked By: JKF

# AWC NDS-18: ASD Member Wood Code Checks (Continued)

	LC	Membe	r Shape	UC Max	Loc[ft]	Shear UC	Loc[ft]	Dir	Fc' [ksi]	Ft' [ksi]	Fb1' [ksi]	Fb2' [ksi]	Fv' [ksi]	RB	CL	CP	Eqn
52	4	M28	6.75X18FS	0.139	0	0.176	2.6	У	2.539	1.76	3.831	2.32	0.48	3.5110			
53	4	M29	6.75X18FS	0.008	0	0.016	0	У	2.539	1.76	3.831	2.32	0.48	3.5110			
54	4	M3	6.75X9FS	0.22	9.75	0.027	9.75	У	1.841	1.76	3.822	2.32	0.48	4.807	0.995	0.719	3.9-1
55	4	M4	6.75X9FS	0.22	0	0.027	9.75	У	1.841	1.76	3.822	2.32	0.48	4.807	0.995	0.719	3.9-1
56	4	M5	6.75X9FS	0.186	0	0.012	9	٧	2	1.76	3.823	2.32	0.48	4.619			
57	5	M2	6.75X9FS	0.032	9	0.002	9	V	1.438	1.1	2.394	1.45	0.3	4.619	0.997	0.899	3.9-1
58	5	M20	6.75X18FS	0.001	2.6	0.003	2.6	٧	1.592	1.1	2.396	1.45	0.3	3.5110	0.999	0.995	3.9-1
59	5	M21	6.75X18FS	0.024	2.6	0.03	0	٧	1.592	1.1	2.396	1.45	0.3	3.5110	0.999	0.995	3.9 - 3
60	5	M22	6.75X18FS	0.031	6.284	0.007	0	y	1.541	1.1	2.391	1.45	0.3	5.4580	0.996	0.963	3.9-3
61	5	M23	6.75X18FS	0.031	0	0.011	9.75	y	1.39	1.1	2.385	1.45	0.3	6.799	0.994	0.869	3.9-3
62	5	M24	6.75X18FS	0.035	10.563	0.019	10.563		1.327	1.1	2.384	1.45	0.3	7.076	0.993	0.829	3.9-3
63	5	M25	6.75X18FS	0.035	0	0.019	0	٧	1.327	1.1	2.384	1.45	0.3	7.076	0.993	0.829	3.9-3
64	5	M26	6.75X18FS	0.031	9.75	0.011	0	V	1.39	1.1	2.385	1.45	0.3	6.799	0.994	0.869	3.9-3
65	5	M27	6.75X18FS	THE RESERVE OF THE PERSON NAMED IN	0	0.007	6.284	v	1.541	1.1	2.391	1.45	0.3	5.458	0.996	0.963	33.9-3
66	5	M28	6.75X18FS	0.024	0	0.03	2.6	٧	1.592	1.1	2.396	1.45	0.3	3.5110	0.999	0.995	53.9-3
67	5	M29	6.75X18FS		0	0.003	0	V	1.592	1.1	2.396	1.45	0.3	3.511	0.999	0.995	3.9-1
68	5	M3	6.75X9FS	0.038	9.75	0.005	9.75	V	1.391	1.1	2.393	1.45	0.3	4.807	0.997	0.869	3.9-1
69	5	M4	6.75X9FS	0.038	0	0.005	9.75	V	1.391	1.1	2.393	1.45	0.3	4.807	0.997	0.869	3.9-1
70	5	M5	6.75X9FS	0.032	0	0.002	9	У	1.438	1.1	2.394	1.45	0.3	4.619			
71	6	M2	6.75X9FS	0.025	9	0.003	9	У	2	1.76	3.823	2.32	0.48	4.619	0.996	0.781	13.6.3
72	6	M20	6.75X18FS	0.002	2.6	0.004	2.6	V	2.539	1.76	3.831	2.32	0.48	3.511			S. 1997 P. C. 1997
73	6	M21	6.75X18FS		2.6	0.043	0	٧	2.539	1.76	3.831	2.32	0.48	3.511	0.998	0.992	23.9-1
74	6	M22	6.75X18FS	0.059	6.218	0.009	0	V	2.382	1.76	3.816	2.32	0.48	5.458			
75	6	M23	6.75X18FS		0	0.015	9.75	v	1.841	1.76	3.8	2.32	0.48	6.799	0.99	0.719	3.9-1
76	6	M24	6.75X18FS	0.062	10.563	0.027	10.563	_	1.663	1.76	3.796	2.32	0.48	7.076	0.989	0.65	3.9-1
77	6	M25	6.75X18FS		0	0.027	0	V	1.663	1.76	3.796	2.32	0.48	7.076	0.989	0.65	3.9-1
78	6	M26	6.75X18FS		9.75	0.015	0	y	1.841	1.76	3.8	2.32	0.48	6.799			
79	6	M27	6.75X18FS	THE RESIDENCE OF THE PARTY OF T	0.065	0.009	6.284	٧	2.382	1.76	3.816	2.32	0.48	5.458	0.994	0.93	3.9-1
80		M28	6.75X18FS		0	0.043	2.6	V	2.539	1.76	3.831	2.32	0.48	3.511			
81	6	M29	6.75X18FS	EXPOSULUTING LINUX VERY	0	0.004	0	У	2.539	1.76	3.831	2.32	0.48	3.511			
82	6	M3	6.75X9FS	0.027	9.75	0.007	9.75	٧	1.841	1.76	3.822	2.32	0.48	4.807	0.995	0.719	93.9-3
83		M4	6.75X9FS	0.027	0	0.007	9.75	٧	1.841	1.76	3.822	2.32	0.48	4.807			
84	6	M5	6.75X9FS	0.025	9	0.003	9	У	2	1.76	3.823	2.32	0.48	4.619			
85		M2	6.75X9FS	0.396	9	0.025	9	V	1.607	1.265	2.752	1.667	0.345	4.619			
86	7	M20	6.75X18FS		2.6	0.033	2.6	V	1.829	1.265	2.755	1.667	0.345	3.511			
87	7	M21	6.75X18FS		2.6	0.375	0	v	1.829	1.265	2.755	1.667	0.345	3.511			
88	7	M22	6.75X18FS		6.284	0.083	0	V	1.759	1.265	2.748	1.667	0.345	5.458			
89		M23	6.75X18FS		0	0.135	9.75	v	1.536	1.265	2.74	1.667	0.345	6.799			
90	7	M24	6.75X18FS		10.563	0.232	10.563		1.444	1.265	2.739	1.667	0.345				53.9-3
91	7	M25	6.75X18FS		0	0.232	0	V	1.444	1.265	2.739	1.667	0.345	7.076			
92	7	M26	6.75X18FS		9.75	0.135	0	y V	1.536	1.265	2.74	1.667	0.345	6.799			
93		M27	6.75X18FS		0	0.083	6.284	y	1.759	1.265	2.748	1.667	0.345		Water Sport of Physics	St. Brack Street Land Control	63.9-3
94		M28	6.75X18FS		0	0.375	2.6	V	1.829	1.265	2.755	1.667	0.345				43.9-3
95		M29	6.75X18FS	CHARLEST VEHICLES IN	0	0.033	0	У	1.829	1.265	2.755	1.667	0.345	3.511			
96		M3	6.75X9FS	0.47	9.75	0.058	9.75	У	1.536	1.265	2.751	1.667	0.345				53.9-1
97		M4	6.75X9FS	0.47	0	0.058	9.75	У	1.536	1.265	2.751	1.667	0.345	4.807	TAC SECURITY TO SECURITY	and the second second	A DE LEGIS POPULATION
98		M5	6.75X9FS	0.396	0	0.025	9	V	1.607	1.265	2.752	1.667	0.345	4.619			
00	1 /	1010	10.70/1010	0.000		0.020			1					1	_	-	

#### **Envelope Node Reactions**

	Node Labe	I	X [k]	LC	Y [k]	LC	Z [k]	LC	MX [k-ft]	LC	MY [-lft]	LC	MZ [k-ft]	LC
1	N11	max	0	7	0	7	0	7	0	7	0	7	0	7
2	7	min	0	1	0	1	0	1	0	1	0	1	0	1
3	N9	max	0	7	0	7	0	7	0	7	0	7	0	7
4		min	0	1	0	1	0	1	0	1	0	1	0	1
5	N1	max	0	6	12.305	7	0	7	0	7	0	7	0	7



Company : MC Squared Designer : Will Witkop Job Number : 2022-0507

Model Name: GOODWIN CHURCH GYM

10/10/2022 4:30:37 PM

Checked By: JKF

### Envelope Node Reactions (Continued)

	Node Label		X [k]	LC	Y [k]	LC	Z [k]	LC	MX [k-ft]	LC	MY [-lft]	LC	MZ [k-ft]	LC
6		min	0	2	-1.975	6	0	1	0	1	0	1	0	1
7	N5	max	0	7	0	7	0	7	0	7	0	7	0	7
8		min	0	1	0	1	0	1	0	1	0	1	0	1
9	N4	max	0	7	12.305	7	0	7	0	7	0	7	0	7
10		min	0	1	-1.975	6	0	1	0	1	0	1	0	1
11	Totals:	max	0	6	24.61	7	0	7						
12		min	0	2	-3.949	6	0	1				1		

**Envelope Node Displacements** 

	Node Label		X [in]	LC	Y [in	] LC	Z [in]	LC	X Rotation [rad]	LC	Y Rotation	[ <b>L</b> £6d]	Z Rotation [rad]	LC
1	N1	max	0	2	0	6	0	7	0	7	0	7	1.459e-3	6
2		min	0	6	0	7	0	1	0	1	0	1	-9.157e-3	7
3	N2	max	0.131	7	0.111	6	0	7	0	7	0	7	2.124e-4	6
4		min	-0.021	6	-0.698	7	0	1	0	1	0	1	-1.323e-3	7
5	N3	max	0.214	7	0.111	6	0	7	0	7	0	7	1.323e-3	7
6		min	-0.034	6	-0.698	7	0	1	0	1	0	1	-2.124e-4	6
7	N4	max	0.345	7	0	6	0	7	0	7	0	7	9.157e-3	7
8		min	-0.055	6	0	7	0	1	0	1	0	1	-1.459e-3	6
9	N5	max	0.172	7	0.079	6	0	7	0	7	0	7	0	7
10		min	-0.028	6	-0.494	7	0	1	0	1	0	1	0	6
11	N6	max	0.017	6	0.263	7	0	7	0	7	0	7	1.455e-3	6
12		min	-0.11	7	-0.042	6	0	1	0	1	0	1	-9.131e-3	7
13	N7	max	0.454	7	0.263	7	0	7	0	7	0	7	9.131e-3	7
14		min	-0.072	6	-0.042	6	0	1	0	1	0	1	-1.455e-3	6
15	N8	max	0.282	7	0.111	6	0	7	0	7	0	7	6.116e-4	6
16		min	-0.045	6	-0.697	7	0	1	0	1	0	1	-3.834e-3	7
17	N9	max	0.151	7	0.118	6	0	7	0	7	0	7	1.47e-3	7
18		min	-0.024	6	-0.741	7	0	1	0	1	0	1	-2.348e-4	6
19	N10	max	0.29	7	0.119	6	0	7	0	7	0	7	2.171e-3	7
20		min	-0.046	6	-0.746	7	0	1	0	1	0	1	-3.451e-4	6
21	N11	max	0.194	7	0.118	6	0	7	0	7	0	7	2.348e-4	6
22		min	-0.031	6	-0.741	7	0	1	0	1	0	1	-1.47e-3	7
23	N12	max	0.055	7	0.119	6	0	7	0	7	0	7	3.451e-4	6
24		min	-0.009	6	-0.746	7	0	1	0	1	0	1	-2.171e-3	7
25	N13	max	0.063	7	0.111	6	0	7	0	7	0	7	3.834e-3	7
26		min	-0.01	6	-0.697	7	0	1	0	1	0	1	-6.116e-4	6
25 26 27	N15	max	0.172	7	0.081	6	0	7	0	7	0	7	0	7
28		min	-0.028	6	-0.506	7	0	1	0	1	0	1	0	6
29	N16	max	0.108	7	0.042	6	0	7	0	7	0	7	1.338e-3	6
30		min	-0.017	6	-0.261	7	0	1	0	1	0	1	-8.395e-3	7
31	N17	max	0.237	7	0.042	6	0	7	0	7	0	7	8.395e-3	7
32		min	-0.038	6	-0.261	7	0	1	0	1	0	1	-1.338e-3	6

Envelope Node Reactions - Overstrength or Capacity Limit

No Data to Print...

# MC SQUARED, INC.

OLYMPIA, WASHINGTÓN 98506 (360) 754-9339 FAX (360) 352-2044 Job: 2022 -0507

Date: 10/10/2022 By: WILL WITKOP

Sheet: HANK INSON FORMULA Page of

	Sheet: MHNK NSON	PORTITOLA	Page	of
				000000000000000000000000000000000000000
Z' = Z' Z'				
$Z_{\parallel}^{\prime} S N^{2} \Theta + Z_{\parallel}$	Z'(052A			
Z <sub>11</sub> S110 0 1 2				
7' - 2740 12	CNDS TABLE	177		
Z, = 3340 LB	CNUS THOLE	121)		
Z'_ = 1890 LB				
AT NODE 16	I = I = (compose	CION		
(-) = (4)	1. ZKIP (COMPRES	310.09		
(10) 34" b 22.	-18.8 KIP (TENSION)			
Boots				
4.0 KIP (COMPRI	ESS10N)			
717.2 K	IP			
77.77.2 K				
18.8 KIP 17.6 KIP				
70.0				
= 6.65/6.6	0210			
	=83.1°			
Z'= (3340 LB) (	22 12)			
Z'= (3340 LB) (	1890LB)		902	13
				BOLT
3340 LB (51M	2 83.1) + 1890 (cos2	83.1)		
×10 BOLTS = 19.02	. KIP > 6.65 K/	PV		

MC SQUARED, INC.
OLYMPIA, WASHINGTON 98506
(360) 754-9339
FAX (360) 352-2044

Job:	
Date	By:

Sheet:	Page	of	

$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	123°	6.7 (COMPESSION)  3/4"&BOLTS (COMPRESSION)		
$Z_{b}^{1} = \frac{(3340 \text{ LB})(1890 \text{ LB})}{3340(51N^{2}B4)} + 1890(\cos^{2}84)$ $Z_{b}^{1} = \frac{(3380 \text{ LB})(1890 \text{ LB})}{3340(51N^{2}B4)} + 1890(\cos^{2}84)$ $Z_{b}^{1} = \frac{(3340 \text{ LB})(1890 \text{ LB})}{3340(51N^{2}B4)} + 1890(\cos^{2}84)$				
$Z_{b}' = \frac{(3340 \text{ LB})(1890 \text{ LB})}{3340(51N^{2}B4) + 1890(\cos^{2}84)} = 1899 \text{ LB}$ $3340(51N^{2}B4) + 1890(\cos^{2}84)$ $BOLT$	VC . #6	KIP	840	38
x2 BOLTS= 3.80 KIP > .38 KIP	Z' = (3340 LB)	(1890 LB)	= 1899	LB BOLT
	x2 BOLTS= 3.80	KIP > .38 KIP	7	

MC SQUARED, INC. OLYMPIA, WASHINGTON 98506 (360) 754-9339 FAX (360) 352-2044

Job:			
Date:	By:	······································	

	Sheet:	rage	01
AT NODE 5			
	14" BOLTS		
-			
67° 67°	11471.0		
6.147 KIP58(T)	6.147 KIP		
- (c)58(T)			
- 67 2.4 KIP+	+ 2.4 kip		
	58 kjp		
5.7 KIP	5.7 kp		
670			
4.2 KIP			
	4		
$= \frac{2}{26} = \frac{(3340 \text{ LB})(186)}{3340 \text{ LB}(5\text{M}^267)}$	(0LB) = 2024	BOLT	
3340 LB(SM267)	+ 1890(cos267)	804	
- XZO BOLTS = 40.5	KIP > 4.2 KIP		
_			

# MC SQUARED, INC.

OLYMPIA, WASHINGTÓN 98506 (360) 754-9339 FAX (360) 352-2044

Job:	
Date:	By:

Sheet:\_\_\_\_\_\_\_\_of\_\_\_\_\_\_

AT NODE 2 102 (4)	
-6.54(c) < -0.54(c) $-1.02(c)  (0) 3/4"  Bats$	
$90^{\circ} \longrightarrow F_{\perp} = 1890 \text{ LB}$	
* 10 BOLTS = 18.9 KIP > . 102 KIP	
AT NODE 9 .414 (T)	
-6.54(c) -6.54 (c)	
(Z) 3/4" \$ 8027S	
.414 KIP	
90'-> F' = 1890 LB/BOLT	
XZ BOLTS = 3.78 KIP >. 414 KIP	

MC SQUARED, INC. OLYMPIA, WASHINGTON 98506 (360) 754-9339 FAX (360) 352-2044

Date:By:	

	Sneet:	Pageoi
DEFLECTION -MAXIMUM	ALLOWABLE DEFLEC	TION
	720 IN = 4 IN	
	AT NODE 15 = . 506	IN < 4/N
_		
-		
_		

Project Title: Engineer: Project ID: Project Descr:

# **Multiple Simple Beam**

Lic. #: KW-06005122

File: 2022-0507 Sanctuary Calculations.ec6 Software copyright ENERCALC, INC. 1983-2020, Build:12.20.10.31

MC SQUARED, INC.

463

0.000 in

9999

LC:

LC: +D+S+H

**Description:** 

### Wood Beam Design: Beams Parallel to the Backwall

Calculations per NDS 2018, IBC 2018, CBC 2019, ASCE 7-16

BEAM Size: 5.5x15, GLB, Fully Braced Using Allowable Stress Design with ASCE 7-16 Load Combinations, Major Axis Bending Wood Species: DF/DF Wood Grade: 24F-V4 Fb - Tension 2,400.0 psi Fc - Prll 1,650.0 psi 265.0 psi Ebend-xx 1,800.0 ksi Density 31.210 pcf Fb - Compr 1,850.0 psi Fc - Perp 1,100.0 psi 650.0 psi Eminbend - xx 950.0 ksi Applied Loads Unif Load: D = 0.0180, S = 0.0250 k/ft, Trib= 8.0 ft <u>Design Summary</u> D(0.1440) S(0.20) Max fb/Fb Ratio = 0.412:1 1,103.30 psi at 10.500 ft in Span # 1 2,680.10 psi fb : Actual : Fb : Allowable : 5.5x15 Load Comb: +D+S+H 21.0 ft Max fv/FvRatio = 0.191:1 58.23 psi at 19.810 ft in Span # 1 304.75 psi fv : Actual : Fv : Allowable : +D+S+H Load Comb: Max Deflections Max Reactions (k) 0.316 in L Lr <u>S</u> W E H Transient Downward **Total Downward** 0.543 in 2.10

Ratio

Ratio

Transient Upward

## Wood Beam Design: Beams perpendicular to the backwall

2.10

Calculations per NDS 2018, IBC 2018, CBC 2019, ASCE 7-16

Ratio

Ratio

**Total Upward** 

8.75x42, GLB, Fully Braced
Using Allowable Stress Design with ASCE 7-16 Load Combinations, Major Axis Bending BEAM Size: Wood Species: DF/DF Wood Grade: 24F-V4 2,400.0 psi Fc - Prll

Fb - Tension 1,650.0 psi 265.0 psi Ebend-xx 1,800.0 ksi Density 31.210 pcf Fb - Compr 1,850.0 psi Fc - Perp 650.0 psi Ft 1,100.0 psi Eminbend - xx 950.0 ksi

Applied Loads

Left Support

Right Support

Unif Load: D = 0.0180, S = 0.0250 k/ft, Trib= 21.0 ft

1.51

1.51

Design Summary Max fb/Fb Ratio = **1.045**: 1 2,156.67 psi at 32.000 ft in Span # 1 2,064.78 psi fb : Actual : Fb: Allowable: Load Comb: +D+S+H **0.346**: 1 105.36 psi a 304.75 psi Max fv/FvRatio = fv: Actual: 0.000 ft in Span # 1 at Fv : Allowable : Load Comb: +D+S+H  $\underline{\mathsf{D}}$ Max Reactions (k) <u>S</u> Ē Ī W 12.10 Left Support 16.80 Right Support

64.0 ft Max Deflections Transient Downward 2.049 in **Total Downward** 3.524 in Н 374 Ratio 217 LC: S Only LC: +D+S+H Transient Upward 0.000 in **Total Upward** 0.000 in Ratio 9999 Ratio 9999 LC: LC:

D(0.3780) S(0.5250)

8.75x42

797

0.000 in

LC:

9999

LC: S Only

PUT SOLAR PANELS ON SANCTUARY

OVER STRESSED